

# Water Supply Assessment for Pumpkinvine Creek Dam No. 2 Bartow County, Georgia



Prepared for:  
**Georgia State Soil and Water Conservation  
Commission**

Prepared by:  
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## EXECUTIVE SUMMARY

The Georgia Soil and Water Conservation Commission (GSWCC), in partnership with the Natural Resources Conservation Service (NRCS) and the Georgia Environmental Protection Division (EPD) initiated a study to evaluate whether or not any of the existing watershed dams, designed and constructed under federal laws PL 544 and PL 566, could be modified to serve as water supply reservoirs. The evaluation process went through several iterations, the most recent of which can be found in the Finding Report dated December, 2007 on file with the GSWCC. The Finding Report identified 20 structures that had sufficient potential for relatively high yields with relatively small environmental and infrastructural impacts, when compared to the other projects evaluated. The selected twenty dams were further evaluated to identify project parameters.

The following report summarizes the evaluation of the Pumpkinvine Creek Dam Number 2, which is located in Bartow County, Georgia. For the purposes of this report, the existing normal pool will be raised to impound a water supply pool having a surface area of approximately 130 acres.

For convenience, the following summary lists the major findings of this evaluation. This summary should not be utilized as a separate document or in lieu of reading the entire report, including the Appendix.

- Approximately 266 acres of land will be impacted by the proposed reservoir and dam raising
- No structures will be impacted by the proposed reservoir and dam raising
- No county roads will be impacted.
- For the modeled conditions, the drought of record in the Pumpkinvine Creek basin is the period 1986-1988. For a water supply storage of approximately 1,240 million gallons and supplementation of natural reservoir inflow by pumped diversions (maximum 11 million gallons per day, mgd) from nearby Pumpkinvine Creek, the safe yield of the reservoir is estimated to be 6.8 mgd.
- Approximately 12 acres of palustrine wetlands will be impacted by the proposed reservoir and dam raising
- Approximately 3 acres of lacustrine/palustrine open waters will be impacted by the proposed reservoir and dam raising
- Approximately 19,896 linear feet of lower perennial streams will be impacted by the proposed reservoir and dam raising
- Approximately 744 linear feet of intermittent streams will be impacted by the proposed reservoir and dam raising
- Review of available information did not indicate any existing identified cultural resources occurring within the maximum reservoir pool limits Pumpkinvine Creek Dam No. 3.
- Review of available resources indicates that one 303(d) listed stream (Ward Creek) is located within the maximum reservoir pool limits of Pumpkinvine Creek 02.
- Eleven protected species, five faunal species and six floral species, are known from Bartow County, Georgia.
- Review of available resources indicates two secondary trout streams are located within the maximum reservoir pool limits of Pumpkinvine Creek 02.
- Project cost is estimated in 2007 dollars at \$78,000,000.

## **PREFACE**

The results of the analyses presented herein are based in part upon United States Geological Survey (USGS) quadrangle maps and, therefore, should be utilized for planning purposes only. If the subject project is identified as having a possibility of progressing past this analysis, additional studies will be required. These studies will include but not be limited to detailed environmental evaluations, detailed yield analyses, preliminary engineering design, and detailed cost estimating. These additional studies will be required prior to beginning detailed design work and/or land acquisition. The level of study presented herein shall be considered as a screening tool to evaluate the proposed project relative to other projects. Until further studies are performed, actual yield and costs associated with the entire project cannot be readily determined.

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## **INTRODUCTION**

The project team of Schnabel Engineering South, LLC (Schnabel), Jordan Jones and Golding (JJ&G), Joe Tanner and Associates, and the Law Office of William Thomas Craig were retained by the Georgia State Investment and Financing Commission as the agent for the Georgia Soil and Water Conservation Commission to evaluate 166 existing flood control structures. The subject structures were originally designed and constructed under Federal laws PL 544 and PL 566 to control storm water runoff (flooding) and collect sediment. The goal of this evaluation was to identify impoundments that could be enlarged to provide a relatively reliable water supply. The results of the evaluation were utilized to select twenty of the dams and reservoirs that had potential for relatively high yields with relatively small environmental and infrastructural impacts, when compared to the other projects evaluated. The selected twenty dams were further evaluated to identify project parameters. The additional evaluation included the following:

- More detailed yield analyses
- More detailed environmental evaluation
- Cost estimation of proposed modifications

The Pumpkinvine Creek Dam No. 2 in Bartow County, Georgia was one of the structures selected for further evaluation.

## **BACKGROUND**

The subject dam, Pumpkinvine Creek Sub-Watershed Coosa River Watershed Dam Number 2 (Pumpkinvine Creek 2), is located approximately 5 miles south of Cartersville, Georgia in Bartow County. More specifically, the dam is located on Ward Creek about 1- $\frac{2}{3}$  miles southwest of the intersection of Old Alabama Road and Bates Road.

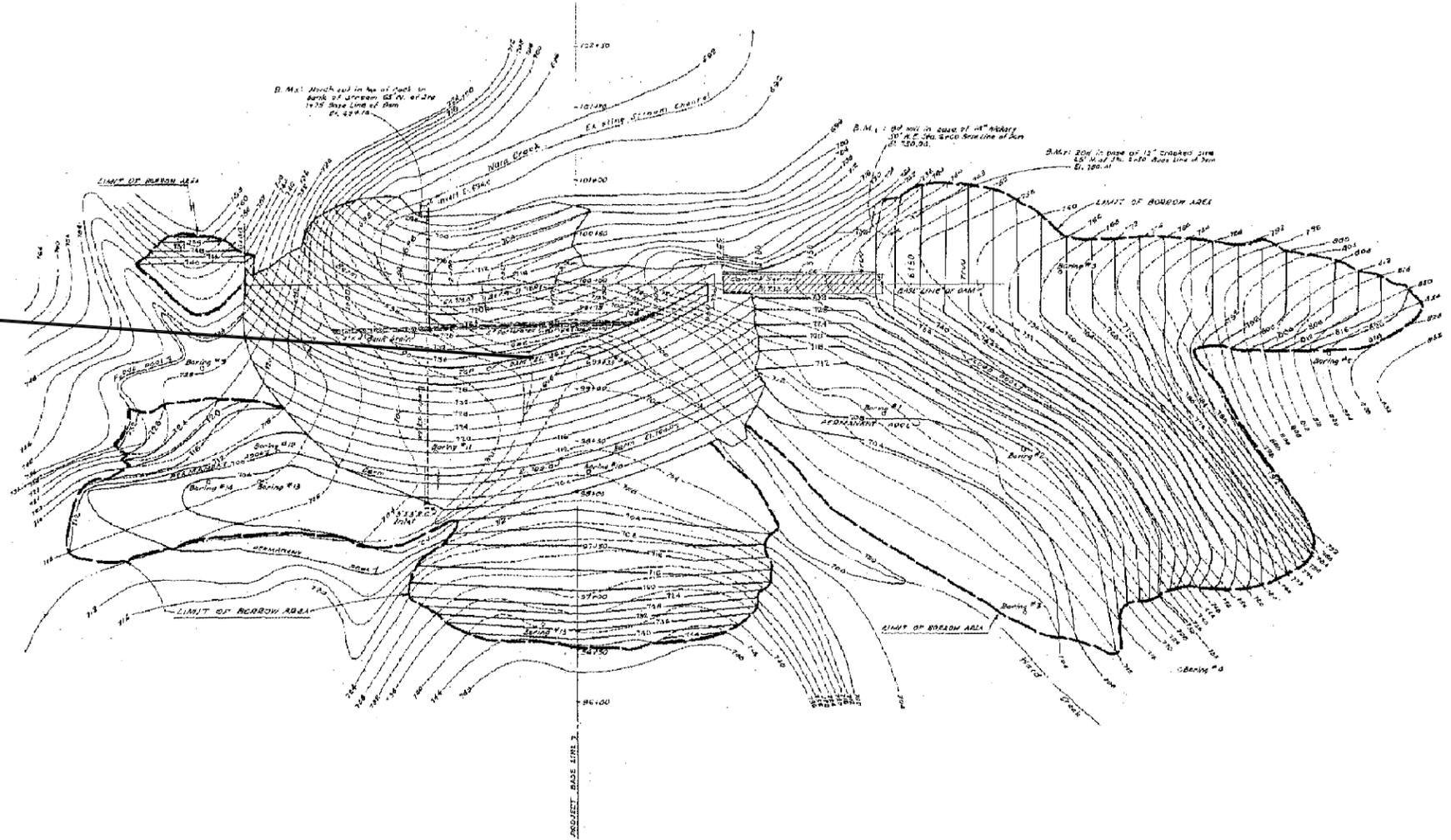
The existing dam was designed in 1954 and constructed in 1955. Recent GIS topography indicates that the existing dam has a crest elevation of approximately 800 feet and impounded a reservoir that had a surface area of approximately 3 acres at a normal pool elevation of approximately 795.0 feet. The topographic information indicates that the crest of the emergency spillway is at an approximate elevation of 796.0 feet. According to the Soil Conservation Service (SCS), now known as the Natural Resources Conservation Service (NRCS), Dam Inventory sheet, the dam was originally designed and constructed as a Class 'A' or low-hazard dam. The state Safe Dams program classifies the existing dam as a Category 2 structure. When designed, the emergency spillway (now referred to as an auxiliary spillway) had a 4 percent chance of operating in any given year. This results in the auxiliary spillway operating during storm events equal to and greater than the 25-year event. Not including engineering, land acquisition, or project administration, the dam was completed for a cost of approximately \$88,000.



PUMPKINVINE CREEK  
NO. 2

**BARTOW COUNTY**

N.T.S.



**EXISTING SITE PLAN**



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NRCS WATERSHED DAM ASSESSMENT  
PUMPKINVINE CREEK NO. 2

SITE LOCATION MAP  
PROJECT NO. 07170030.01  
FIGURE 1

## NEEDS AND DEMAND EVALUATION

Population projections through the year 2030 were obtained from the Bartow County Community Assessment (published in 2006). Projections to 2057 were extrapolated based on the assumption of the same constant growth rate that was shown in the Comprehensive Plan. These projections can be seen in Table 1.

**Table 1**  
**Population Projection**

<b>Year</b>	<b>Population Projection</b>
2000	76,019
2005*	99,602
2010	123,184
2015*	153,978
2020	184,772
2025*	192,403
2030	200,034
2035*	208,296
2040*	216,557
2045*	225,501
2050*	234,444
2055*	244,127
2057*	248,000

*Data Source: from Bartow County Community Assessment*

*\*Population calculated based on yearly % growth from 2000-2030*

Water demand projections were calculated based on population projections and water withdrawal data for Bartow County in 2000. According to the US Census, the population of Carroll County was 76,019 in 2000, while the water withdrawal was 18.1 million gallons per day (MGD) based on the document “Water Use in Georgia by County for 2000”, (Information Circular 106, Julia Fanning, USGS, Atlanta, 2003). The Bartow County Water System currently holds a surface water withdrawal permit of 0.8 MGD from Bolivar Springs. The City of Cartersville holds a surface water permit from the Etowah River for 23 MGD and Lake Allatoona for 18 MGD, and the City of Emerson has a 0.5 MGD permit from Moss Springs. In addition to the surface water permits, the City of White holds a groundwater withdrawal permit for 0.2 MGD. All totaled, water withdrawal permitted for public use in Bartow County is 46.6 MGD (all numbers are reported in permitted monthly average).

The overall usage was calculated to be 239 gallons per day (gpd) per person. This number was used as a constant through 2057 to create water withdrawal projections. The water withdrawal projection for 2057 was calculated to be approximately 59 MGD. This figure includes all unaccounted for water (UAW), and the assumption that industrial usage would increase with the increase in Bartow County population. Water withdrawal projections are shown in Table 2.

**Table 2**  
**Water Withdrawal Projection**

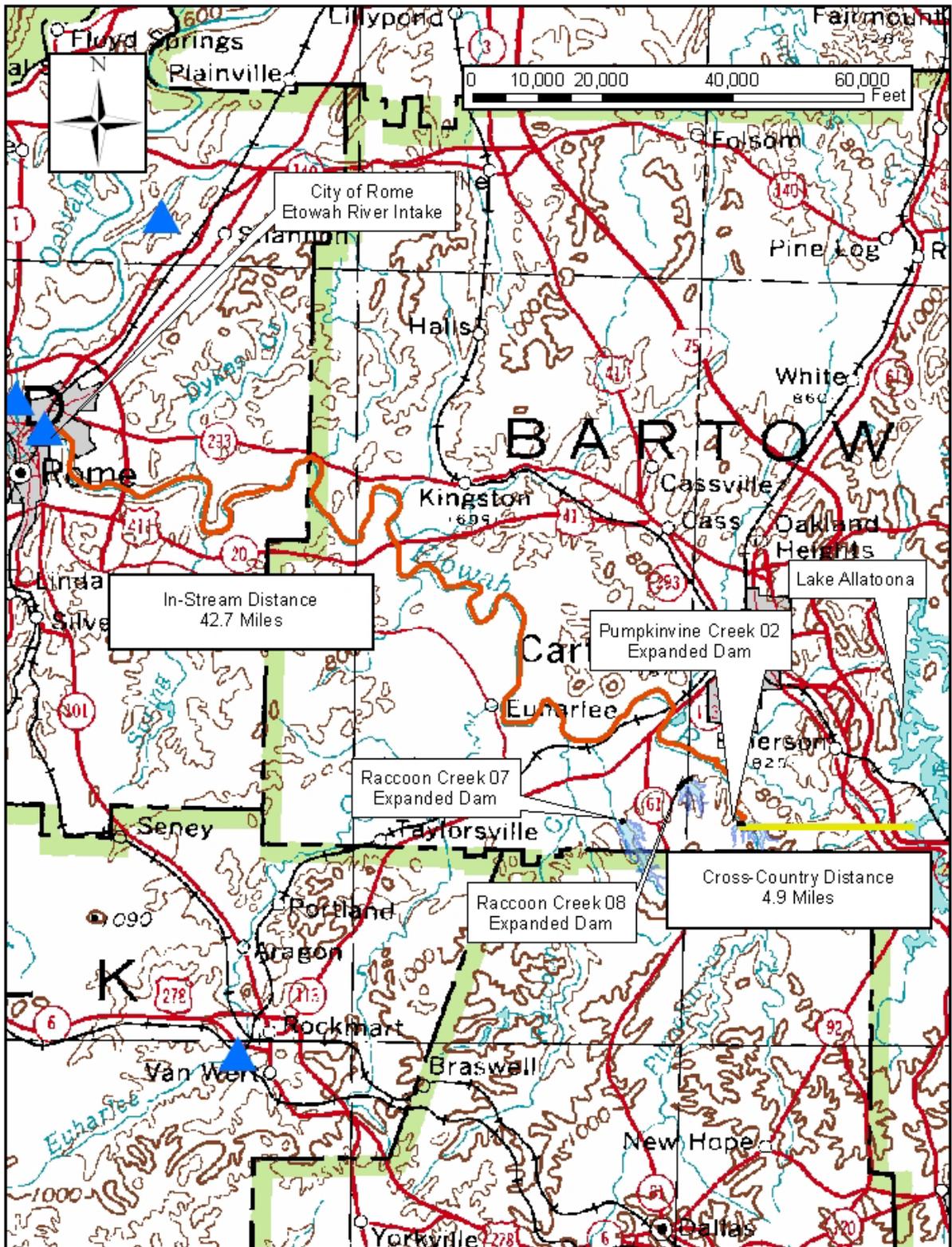
<b>Year</b>	<b>Water Withdrawal Projection (MGD)</b>
2000	18
2005	24
2010	29
2015	37
2020	44
2025	46
2030	48
2035	50
2040	52
2045	54
2050	56
2055	58
2057	59

**Proximity to Surface Water Intakes**

Based on the GIS database developed for this project, the closest downstream surface water intake structure is 42.7 miles downstream of the dam on the Etowah River. This structure is operated by the City of Rome. The Etowah River is approximately 2.4 miles from the dam along Ward Creek. The remaining 40.3 miles is along the Etowah River.

Lake Allatoona is approximately 4.9 miles to the east of the dam. Figure 2 illustrates the locations of the nearest surface water intakes to Pumpkinvine Creek 02.

**Figure 2**  
**Distance to Nearest Intake**



## ENGINEERING FACTORS

### Proposed Dam

The proposed dam, which will incorporate the existing dam, has a crest elevation of 860 feet, an auxiliary spillway elevation of 845 feet, and a normal pool elevation of 842 feet. The proposed dam will impound a reservoir that has a surface area of approximately 130 acres and storage volume of approximately 1,240 million gallons (MG). A plan view of the proposed reservoir is shown in Figure 3.

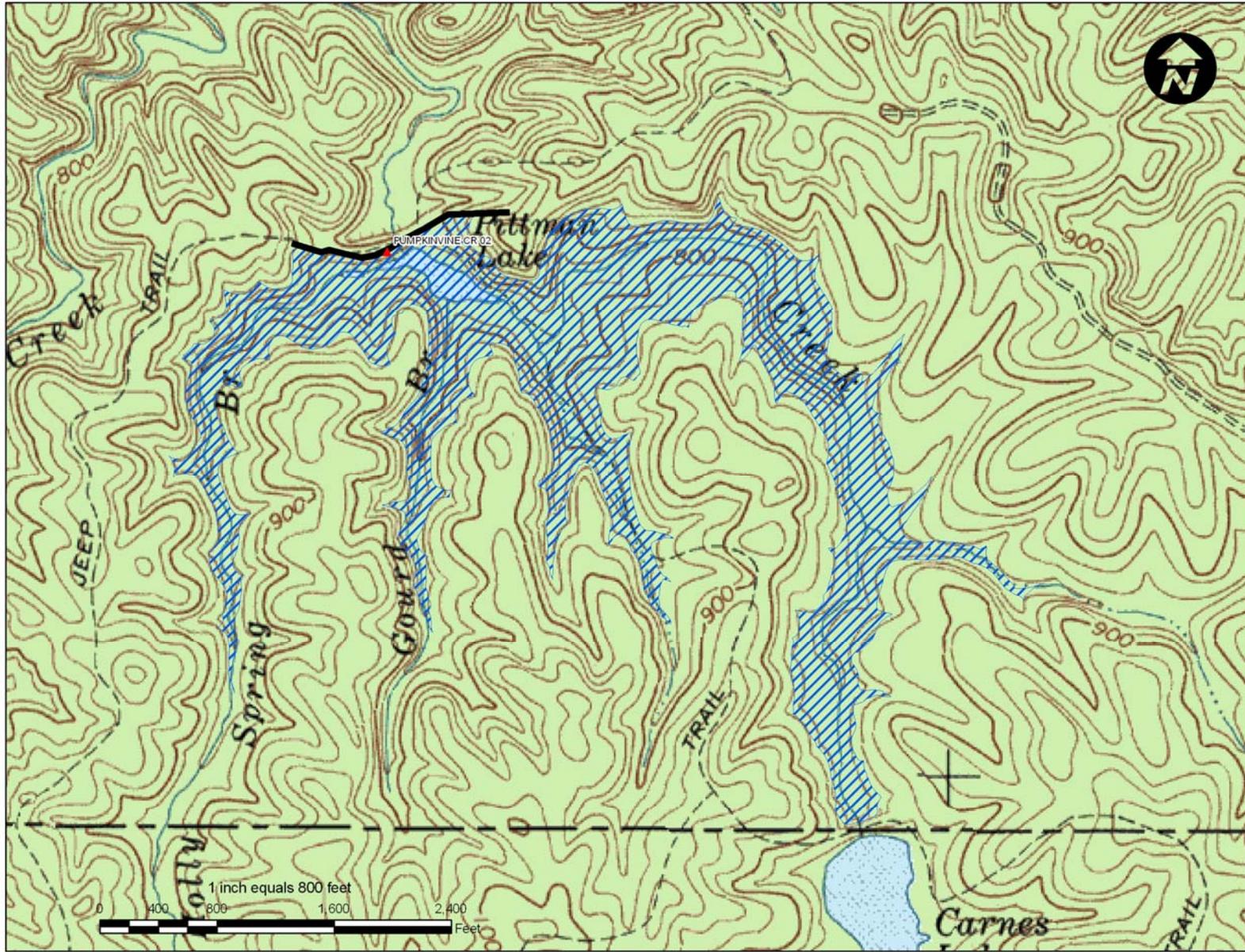
Several engineering assumptions were made pertaining to spillway configuration. The spillway system for the proposed dam was assumed to consist of a principal spillway in the form of a 3' by 3' interior dimension reinforced concrete riser with a 24-inch diameter reinforced concrete low-level outlet pipe and an auxiliary spillway in the form of a 120-foot wide reinforced concrete chute spillway with ogee crest. The intent of the proposed principal spillway is to approximate the flows that are being discharged by the current spillway system during the two through 100-year storm events. The size of the auxiliary spillway was approximated by estimating the peak inflow that would occur during the Probable Maximum Precipitation (PMP) event and computing the spillway width that would be required to pass the estimated inflow with a given amount of hydraulic head. The available hydraulic head was determined by comparing the drainage basin area to lake surface area. The structures that had a drainage basin area to lake surface area ratio equal to or in excess of ten were allotted 15 feet of hydraulic head to pass the PMP inflows, while the structures that had a ratio of less than ten were allotted ten feet of hydraulic head to pass the PMP inflows. The assumption that the dam would be required to pass the inflow resulting from the PMP storm event is based on the history of the Georgia Department of Natural Resources Environmental Protection Division Safe Dams Program (Safe Dams) reviewing plans for water supply reservoir dams regardless of classification. As such, the dam would generally be required to comply with the engineering guidelines established by Safe Dams. Based upon the height of the dam (approximately 112 feet), the dam would be required to store and/or pass the inflows from the full PMP event safely. Additionally, the proposed dam would have a relatively high likelihood of being classified as high-hazard or Class 'C' by the NRCS, as well as Safe Dams.

The proposed dam and flood pool will:

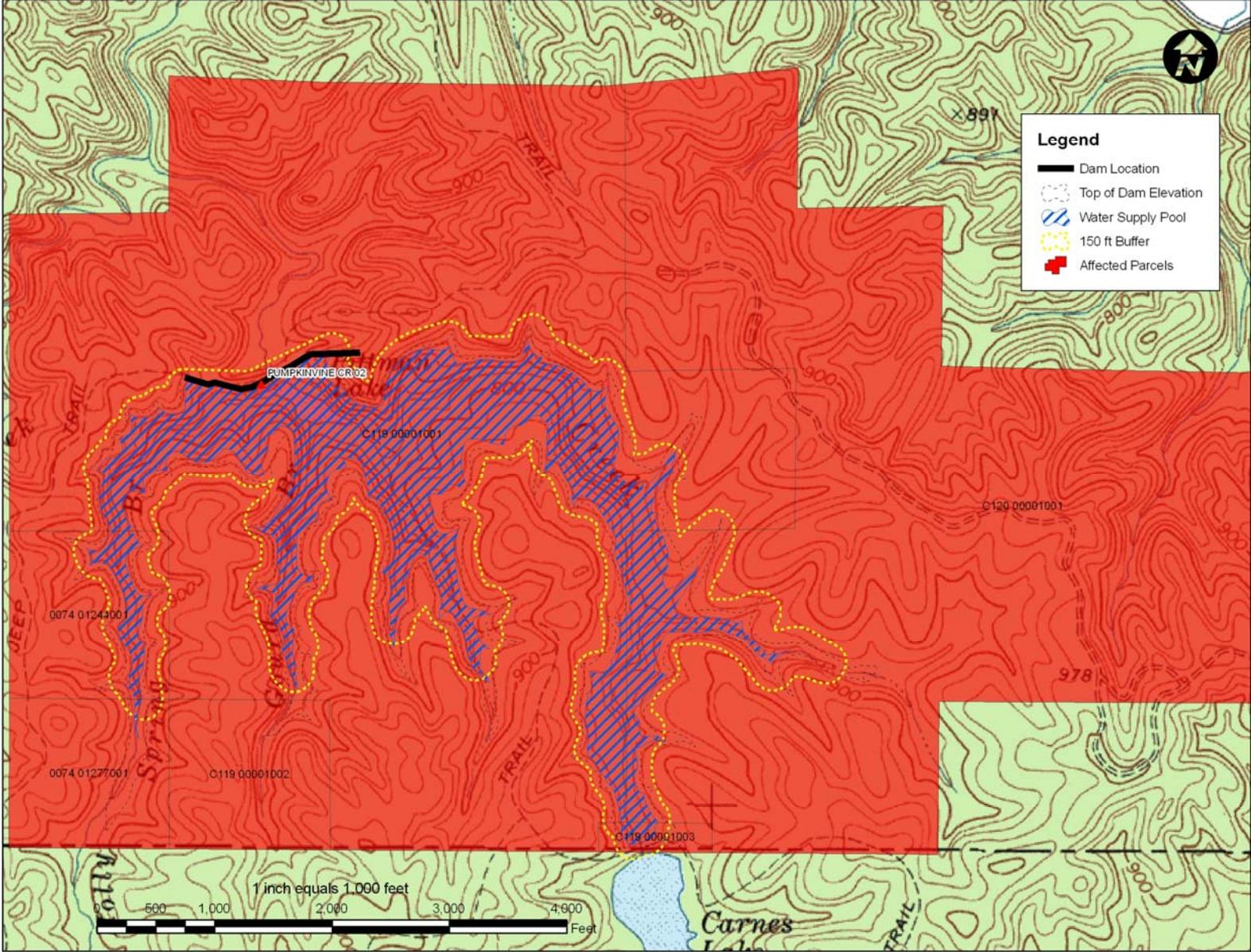
- Impact no structures
- Require the purchase of 189 acres from 6 parcels
- Require the purchase of 77 acres of easement area for state required buffer
- Impact no local/county roads

Figure 4 displays the proposed reservoir area as well as the buffer and affected parcels.

Figure 3  
Proposed Reservoir Area Map



**Figure 4**  
**Land Acquisition and Buffer Areas**



## SAFE YIELD ANALYSIS

### Definition

Reservoir safe yield is generally defined as the reliable withdrawal rate of water with acceptable quality that can be provided by reservoir storage through the critical drought period. The critical drought period in the State of Georgia is defined as the drought of record and in any given drainage basin can vary depending on reservoir size and other factors. This study was based on the critical drought period from 1986-1988; however, the current drought could possibly exceed the existing drought of record. If this were to occur, the computed yields detailed herein would be reduced. Safe yield in this study was simulated using a constant average annual demand. The justification for this is that while total water demands after declaration of a drought condition are usually less than normal, this situation is typically offset by higher than average demands prior to declaration of the drought condition. Safe yield is dependent upon the storage and hydrologic (rainfall/runoff/evaporation) characteristics of the source and source facilities, the selected critical drought, upstream and downstream permitted withdrawals, and the minimum in-stream flow requirements.

The proposed reservoir is a “pumped-storage” reservoir, where natural inflow into the reservoir is supplemented with pumped diversions from a nearby larger stream or river. Water is pumped from a larger river when runoff is plentiful, and is stored in the reservoir for times of drought. Pumped diversions increase safe yield, and generally result in fewer environmental impacts compared with reservoirs on main-stem rivers.

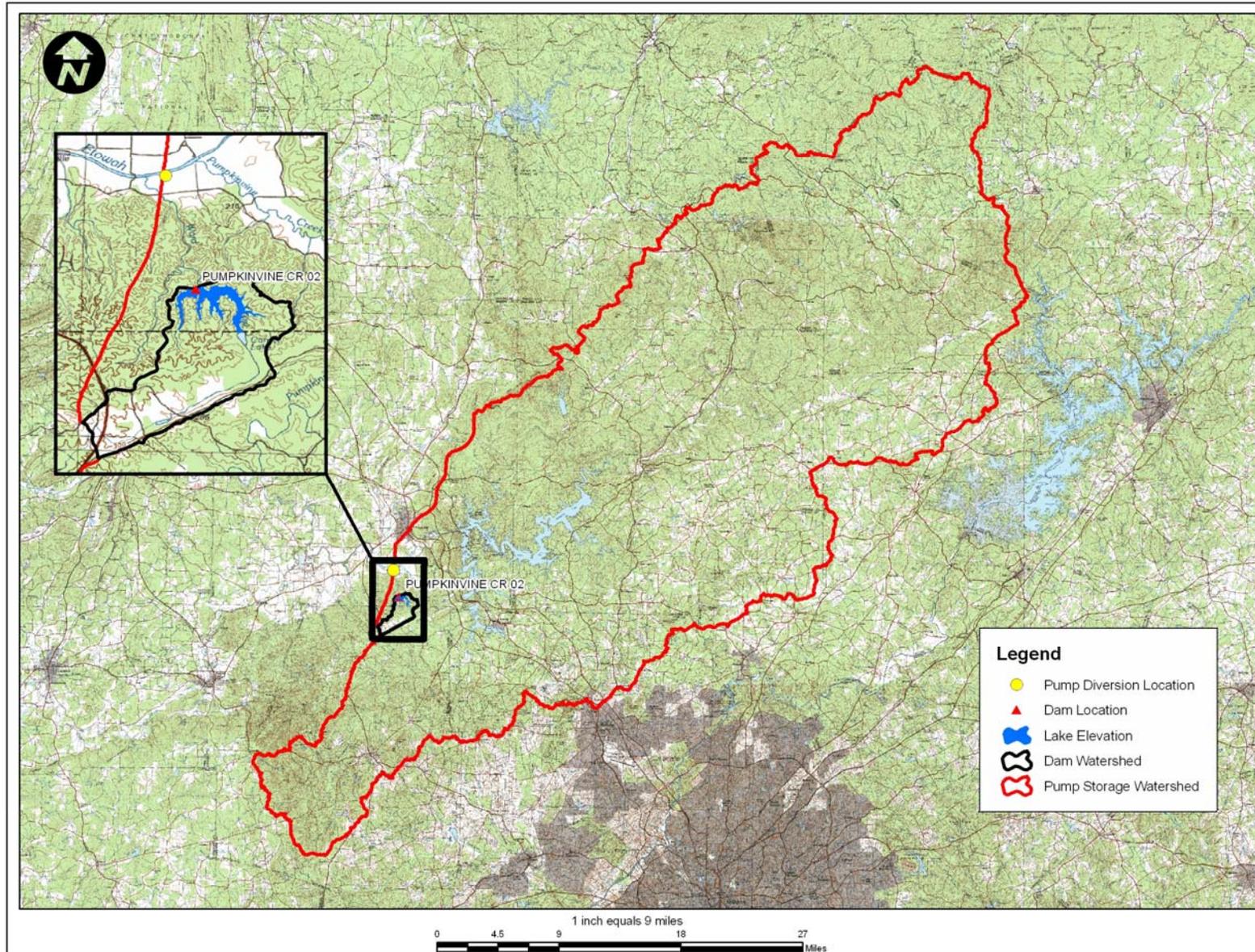
### Analysis Method

Two sets of stream flow data were used for the safe yield analysis. For simulation of available flow for pumped diversions from the Etowah River, the following gage was used: Etowah River At Allatoona Dam above Cartersville, GA (USGS 02394000). For simulation of flow directly to the proposed reservoir and the intervening drainage area between Allatoona Dam and the proposed pump station, the Two Run Creek near Kingston (USGS 02395120) gage was selected for use. The record period for the Two Run Creek gage extends from May 1980 to present, while the record period for the Etowah River gage extends from 1938 to present. Therefore the overlapping period of 1980 to present was used in the analysis, which includes two major droughts (1986-88 and 1999-2002), plus the current drought. The diversion pump station was assumed to be located just upstream of the confluence of Ward Creek with the Etowah River. The straight line pipe distance between the dam and diversion location was estimated at 1.6 miles. The following drainage areas were used in the analysis:

- Dam Site (Ward Creek): 4.20 mi<sup>2</sup>
- Diversion (Etowah River): 1274 mi<sup>2</sup>

The pumped diversion location and watershed is shown in Figure 5. The maximum estimated pool level at top of dam was selected during the initial screening phase based on USGS topographic mapping. Subsequently more detailed GIS topographic data was obtained for calculation of reservoir storage. A freeboard allowance of 15 feet between the top of dam and the auxiliary spillway was incorporated to pass the spillway design flood (assumed to be the probable maximum flood).

**Figure 5**  
**Watershed Location Map**

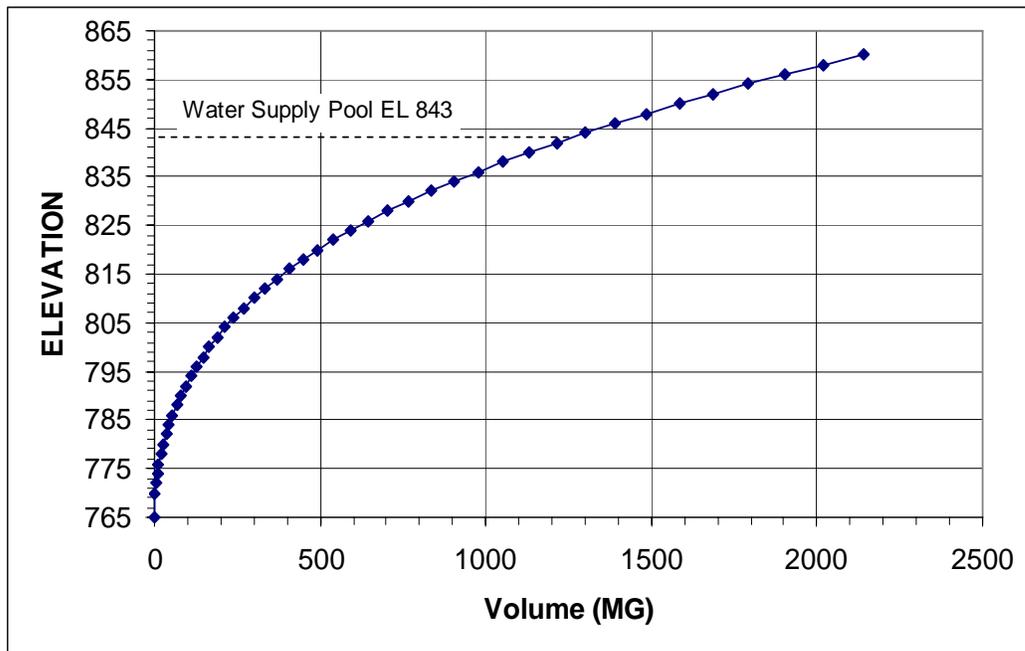


Additional depth to maintain existing flood storage volume (345 Ac-ft, or 112 MG) was subtracted from the auxiliary spillway elevation to compute the water supply pool elevation used in the analysis of safe yield. Table 3 summarizes the various reservoir elevations and approximate storage volumes. Calculation of stage-area and stage-storage curves is presented as Figure A-1a and A-1b in the Appendix. Figure 6 below is the stage-storage curve for the reservoir.

**Table 3**  
**Summary of Reservoir Data**

Stage	Elevation	Volume (Million Gallons)
Maximum Pool (Top of Dam)	860	2,140
Flood Pool (Auxiliary Spillway Crest)	845	1,350
Water Supply Pool	843	1,240

**Figure 6**  
**Stage-Storage Curve**



A reservoir operations model was developed to incorporate daily gage data from the selected USGS gage and reservoir shape parameters for estimation of evaporation. The following assumptions were incorporated into the analysis for the estimation of safe yield:

**Assumptions:**

1. Dead storage of 20% of gross reservoir storage was incorporated to allow for sediment storage and poor water quality in lower reservoir strata.
2. Usable water supply storage was assumed to be the water supply pool storage (calculated as noted above) less dead storage.

3. Pump station diversions were assumed to be from Etowah River at the location previously described. Diversions were assumed to occur whenever the reservoir level fell below full water supply pool. Pumped diversions were assumed to be bounded by pumping capacity and by flow restrictions on Etowah River (noted below).
4. A minimum in-stream flow (MIF) of 30% AAF at the diversion pump station (Etowah River) was used.
5. Allowance for downstream withdrawals by the Georgia Power Plant at Bowen, City of Rome, and Inland Rome Inc. would reduce available flow in the stream. In addition to the MIF, the model provided for a prorated let-by with the following characteristics:

<b>Permittee:</b>	<u>Georgia Power</u>	<u>City of Rome</u>	<u>Inland Rome Inc.</u>
<b>Downstream Withdrawal:</b>	59.5 mgd	16.4 mgd	32 mgd
<b>Drainage Area:</b>	1421 mi <sup>2</sup>	4010 mi <sup>2</sup>	4100 mi <sup>2</sup>
<b>Prorated Let-by:</b>	53.34 mgd	5.21 mgd	9.94 mgd

6. Upstream withdrawals in Etowah River basin would reduce available flow in the stream. The model incorporated the upstream withdrawals (between Lake Allatoona and proposed pump station) with the following characteristics:

<b>Permittee:</b>	<u>City of Cartersville</u>	<u>Baroid Drilling Fluids</u>	<u>New Riverside Ochre Company</u>
<b>Upstream Withdrawal:</b>	23 mgd	2.5 mgd*	11 mgd*
<b>Drainage Area:</b>	1132 mi <sup>2</sup>	1122 mi <sup>2</sup>	1122 mi <sup>2</sup>
<b>MIF</b>	none	none	none

\*For modeling purposes, one withdrawal by Baroid Drilling Fluids and two withdrawals by New Riverside Ochre Company, Inc. were combined at an average drainage area of 1122 mi<sup>2</sup>.

7. For the dam site, minimum in-stream flow of 30/60/40 percent average annual flow (AAF) was used. This MIF applies as follows: 30% AAF for July through November; 60% AAF for January through April; and 40% AAF for May, June and December.
8. Return flow from wastewater discharges or septic systems was not considered in the analysis.
9. Evaporation loss was based upon net historical evaporation rates (maximum average day) for each month as recorded at Allatoona Dam (Station No. 181) in Bartow County. Lake evaporation was assumed to be equal to 70% of pan evaporation during each month. Surface area was approximated by a regression equation relating storage to surface area (Figure A-2, Appendix).
10. Streamflow data from the USGS gages was applied in direct proportion of drainage areas to simulate flow into the reservoir and at the diversion location.
11. Total seepage losses would be less than the MIF requirements and, therefore, did not need to be separately considered.
12. Safe yield is that quantity of water that can be provided to meet water demands during the critical drought period.

The attainable safe yield during the analyzed period was found by iteration of the daily mass balance equation:

$$\text{Ending Storage} = (\text{Beginning Storage}) + (\text{Natural Inflow}) + (\text{Pumped Inflow}) - (\text{Water Supply}) - (\text{Evaporation}) - (\text{MIF})$$

The trial safe yield value was varied until the reservoir level just reached the dead storage value, and recovery of the reservoir was computed.

## RESULTS

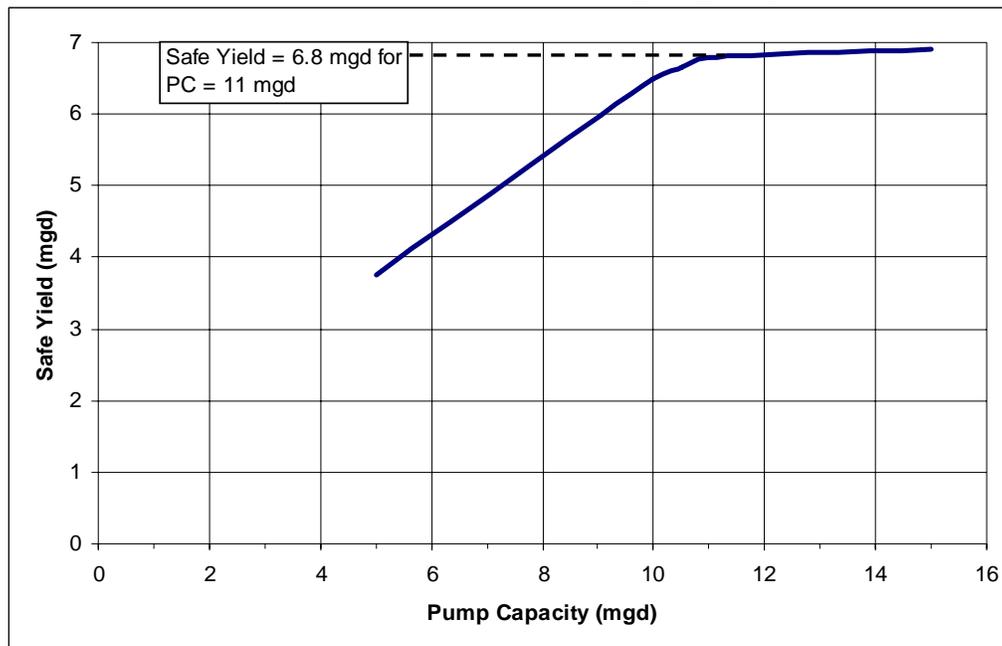
Incorporating the above assumptions, the estimated safe yield of the site was computed. The results of the safe yield analysis are presented in Table 4 and Figure 7. These estimated safe yield values are based on detailed GIS topographic mapping data. The table below presents the estimated safe yield and refill time for a range of pump capacities. We have assumed a refill time of 4 to 5 years is the maximum refill duration for selection of pump capacity (PC).

**Table 4**  
**Safe Yield Summary**

Pump Capacity (MGD)	Estimated Safe Yield (mgd)	Refill Time* (years)
5	3.8	4
10	6.5	3
15	6.9	1

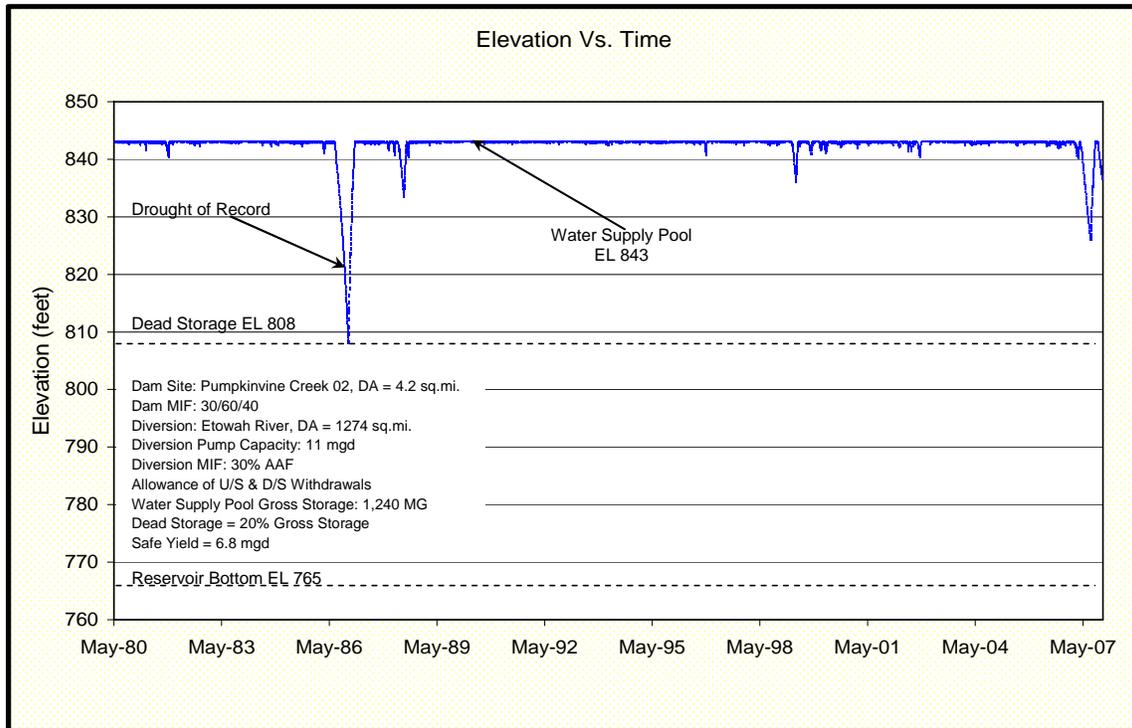
\*Refill time is the time from start of drawdown until complete refill to water supply pool

**Figure 7**  
**Estimated Safe Yield vs Pump Capacity**



As presented in Figure 7, there is diminishing return (safe yield) with increasing pump capacity (reflecting pump station and pipeline cost). For the purposes of this analysis, an estimated economical safe yield & pump capacity combination were selected from the above graph. The estimated safe yield for this project is approximately 6.8 mgd for a pump capacity of 11 mgd. These values were used to size and cost out the diversion facilities detailed later in this report. The variation of reservoir elevation over time for the above assumed safe yield and pump capacity is reflected in Figure 8.

**Figure 8**  
**Reservoir Elevation vs. Time**



## ENVIRONMENTAL CONSIDERATIONS

### Preliminary Studies

To evaluate the potential environmental impacts, permitting requirements, and compensatory mitigation associated with Pumpkinvine Creek 02, preliminary ecological studies were conducted by JJG. These studies consisted of a desktop survey and wetland approximation field surveys to estimate wetlands and streams occurring within the project area. While this evaluation is not sufficient for Clean Water Act Section 404 permitting, field surveys add increased confidence to the desktop evaluation. All estimates of jurisdictional waters, permitting requirements, and compensatory mitigation requirements/cost estimates presented herein are very general and preliminary in nature. Detailed studies would be necessary to definitively determine permitting requirements.

Prior to conducting field surveys, desktop evaluations were performed with available data resources including the U.S. Geological Survey 7.5-minute topographic maps and U.S. Fish and Wildlife Service (USFWS) National Wetland Inventory (NWI) maps. JJG ecologists then performed a reconnaissance-level site visit to the Pumpkinvine Creek 02 site to verify and supplement the desktop evaluation. Subsequent to field surveys, observations were transcribed into an ArcView GIS database for analysis. Preliminary estimates of jurisdictional waters (i.e., wetlands, streams, open waters) occurring within the Pumpkinvine Creek 02 project area are provided below.

### Wetlands

The *Classification of Wetlands and Deepwater Habitats of the United States* (Cowardin Classification System) defines the Palustrine System as all nontidal wetlands dominated by trees, shrubs, persistent emergent vegetation, emergent mosses or lichens, and all such wetlands that occur in tidal areas where salinity is less than 0.5 percent. It also includes wetlands lacking such vegetation, but with all of the following four characteristics: 1) area less than 20-acres; 2) the lack of active wave-formed or bedrock shoreline; 3) water depth in the deepest part of basin less than 6.6 feet at low water; and 4) salinity due to ocean-derived salts less than 0.5 percent.

The Lacustrine System includes wetlands and deepwater habitats with all of the following characteristics: 1) situated in a topographic depression or a dammed river channel; 2) lacking trees, shrubs, persistent emergent vegetation, emergent mosses or lichens with greater than 30-percent areal coverage; and 3) total area exceeds 20 acres. Wetlands and deepwater habitats less than 20-acres are also included in this system if an active wave-formed or bedrock shoreline feature makes up all or part of the boundary, or if the water depth in the deepest part of the basin exceeds 6.6 feet at low water.

Office and field reviews determined that approximately 12 acres of palustrine wetlands and approximately three acres of lacustrine/palustrine open waters exist within the Pumpkinvine Creek 02 project area. These systems are primarily associated with Ward Creek, Holly Springs Branch, Gourd Branch, Pittman Lake, and unnamed tributaries within the proposed reservoir pool limits. Cowardin classifications of the wetland systems range from palustrine forested to palustrine emergent with hydrologic regimes ranging from saturated to seasonally flooded.

### Streams

The Cowardin Classification System defines lower perennial streams as low gradient streams with slow water velocities and substrates comprised mainly of sand and mud. Intermittent streams are defined as streams flowing for only part of the year. When water is not flowing, it may remain in isolated pools or surface water may be absent. Ephemeral streams flow only in direct response to precipitation and do not receive groundwater contributions.

Office and field reviews indicate that approximately 19,896 linear feet of lower perennial streams and approximately 744 linear feet of intermittent streams are located within the maximum reservoir pool limits of Pumpkinvine Creek 02. Ephemeral streams were not identified due to the preliminary nature of the studies. Refer to Figure 9 for locations of these jurisdictional features.

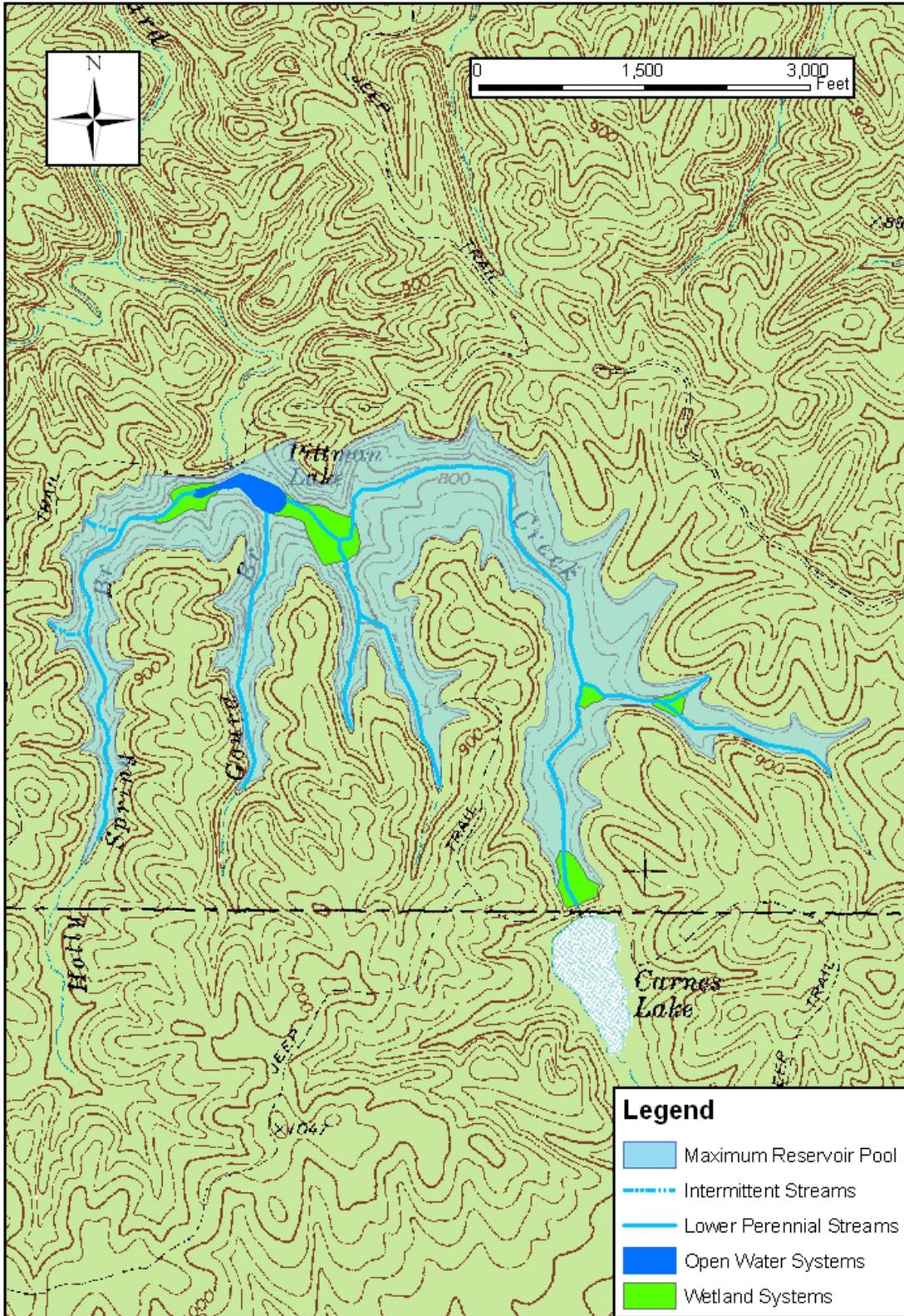
### **Cultural Resources**

Review of existing cultural resources information did not indicate any cultural resource sites within the maximum reservoir pool limits of Pumpkinvine Creek 02. A Phase I Cultural Resources Survey (conducted to the standards of Section 106 of the National Historic Preservation Act) and coordination with Georgia Historic Preservation Division would be required to determine potential Cultural Resources impacts for any proposed reservoir project.

### **Threatened and Endangered Species**

Eleven protected species, five faunal species and six floral species, are known from Bartow County, Georgia. Refer to Table 5 for a summary of protected species located in Bartow County and potential habitat for these species within the maximum reservoir pool limits. Review of existing threatened and endangered species information identified the presence of one protected species. The Georgia Department of Natural Resources – Non-game Conservation Section indicates the occurrence of bay star-vine (*Schisandra glabra*), a state threatened floral species, within the maximum reservoir pool limits of the Pumpkinvine Creek 02 project area in Bartow County, Georgia. Botanical surveys conducted during the growing season are necessary to determine the presence or absence of bay star-vine within the project area.

**Figure 9**  
**Jurisdictional Areas Location Map**



**Table 5**  
**Summary of Protected Species for Bartow County, Georgia**

Scientific Name	Vernacular Name	Federal Status	State Status	Habitat Present (Yes/No)	Preferred Habitat
<b>Fauna</b>					
<i>Lioplax cyclostomaformis</i>	cylindrical lioplax	E	X		mud under large rocks in rapid currents over stream and river shoals; presumed extirpated.
<i>Etheostoma etowahae</i>	Etowah darter	E	E		riffles of clear water streams with moderate to strong current over gravel or cobble substrate; typically associated with swiftest portion of riffles; species is intolerant of impoundment
<i>Etheostoma scotti</i>	Cherokee darter	T	T		shallow water in small to medium creeks with rocky bottoms in the Coosa River Basin
<i>Macrhybopsus</i> sp. 1	Coosa chub	NA	E		swift currents over gravel substrates
<i>Myotis grisescens</i>	gray bat	E	E		restricted to caves or cave-like habitats; forages primarily over water along rivers or lake shores
<b>Flora</b>					
<i>Berberis canadensis</i>	American barberry	NA	E		occurs in open woods, on bluffs and cliffs, and along riverbanks
<i>Crataegus triflora</i>	three-flowered hawthorn	NA	T		hardwood forests on rocky, limestone slopes
<i>Fothergilla major</i>	mountain witch-alder	NA	T		Dry ridgetop forests of middle elevation ridges in the mountains, and in rocky (sandstone, granite) woods; boulder stream margins

**Table 5**  
**Summary of Protected Species for Bartow County, Georgia**

<b>Scientific Name</b>	<b>Vernacular Name</b>	<b>Federal Status</b>	<b>State Status</b>	<b>Habitat Present (Yes/No)</b>	<b>Preferred Habitat</b>
<i>Rudbeckia heliopsidis</i>	Little River black-eyed Susan	NA	T		moist to wet sites (acidic swales in pine-oak woodlands, peaty seeps in meadows, sandy alluvium) with full sun to partial shade
<i>Schisandra glabra</i>	bay star-vine	NA	T		twining in subcanopy and understory trees/shrubs in rich alluvial woods
<i>Xyris tennesseensis</i>	Tennessee yellow-eyed grass	E	E		open or thin canopy woods, seepy margins of limestone seep runs, and banks of small streams or ditches

E= endangered, NA= not applicable, T= threatened, X=presumed extirpated

### **Trout Streams**

Review of available resources indicates two secondary trout streams (Spring Branch and Ward Creek) are located within the maximum reservoir pool limits of Pumpkinvine Creek 02. According to the Georgia Erosion and Sedimentation Act, as amended (Code Section 12-7-6(16)), the state of Georgia prohibits land disturbing activities within 50 feet (horizontally measured) of state waters classified as trout waters, unless a variance is obtained from the Director of the Environmental Protection Division. A completed application form is required by the Environmental Protection Division for evaluating requests for such approval. Please refer to *Rules of Georgia Department of Natural Resources Environmental Protection Division, Chapter 391-3-7 Erosion and Sediment Control, Section 391-3-7.05, Buffer Variance Procedures and Criteria* for a list of activities that do not require an application to or approval from the Division.

### **303(d) and 305(b) Listed Streams**

Review of available resources indicates that one 303(d) listed stream (Ward Creek) is located within the maximum reservoir pool limits of Pumpkinvine Creek 02.

### **Section 404/401 Permitting**

The U.S. Army Corps of Engineers (USACE) regulates the discharge of dredged or fill material into the Nation's Waters under Section 404 of the Clean Water Act. Construction of an impoundment and flooding jurisdictional streams/wetlands is regulated by the USACE. Two types of permits are available through the USACE: Nationwide and Individual Permits. Nationwide Permits (NWP) have been established previously by the Chief of Engineers for projects that have minimal cumulative impacts to the Nation's Waters. Examples of the most

commonly used NWP's include site development, minor road crossings, maintenance activities, and utility line discharges. Specific criteria and conditions were established that must be satisfied prior to obtaining authorization of a NWP from the USACE. In addition, the Savannah District of the USACE issued Final Nationwide Permit Regional Conditions effective May 11, 2007.

Individual Permits (IP) are required for projects having more than minimal cumulative adverse impacts on the Nation's waters. The development of a water supply reservoir would typically require an IP. IPs involve significantly more information, documentation, and coordination with regulatory agencies and are considerably more difficult to acquire than a NWP. Prior to coordination with the USACE regarding the construction of an impoundment, required information would consist of, but not be limited to, the following information:

- Justification of Purpose and Need for the project
- Alternatives analysis of other water supply options evaluated to meet the need
- Wetland delineation with surveyed boundaries of USACE jurisdictional waters
- Phase I cultural resources and protected species surveys
- Detailed description of proposed project and proposed impacts to jurisdictional waters
- Detailed analysis of flow releases documented with population analysis and system modeling
- Avoidance and minimization of jurisdictional waters analysis
- Identification of adjacent property owners
- Development of a conceptual compensatory mitigation plan

Following completion of these items, a complex project meeting would typically be scheduled with the USACE Northern Area Section Office (Morrow, GA) to present the proposed project. Subsequent to the meeting, and if a project is tentatively accepted by the regulatory agencies, formal application and preparation of an IP would start. Following submittal of an IP, the application must be advertised for public comment. The USACE prepares the public notice, which includes detailed applicant information such as site location, proposed impacts, cultural resources, protected species, and proposed mitigation. The public notice would be advertised for 30 days and is also submitted to regulatory agencies including the Environmental Protection Agency (EPA) and USFWS, adjacent property owners, and to the USACE general mailing list. Applicants will be required to respond to inquiries received during the public notice process. Public hearings could be required if substantial adverse comments are received from the coordinating agencies or the public. Additional information and permitting required would consist of a Section 401 Water Quality Certification from the Georgia Environmental Protection Division (EPD). This certification must be issued for an IP to be valid. Depending on the level of impacts associated with the proposed reservoir, an Environmental Assessment or Environmental Impact Statement could be required by the USACE as well. Based on previous project experience, the level of controversy and environmental issues raised during agency and public review, a typical new reservoir project may require permitting times of 5 years or more.

The expansion of an existing reservoir could potentially facilitate the Section 404 permitting process when compared to the construction of a new impoundment. This is especially true for issues such as alternatives analysis, avoidance and minimization, and aquatic organism passage in that many or most potential impacts have already occurred. However, the steps of the overall Section 404 permitting process would still need to be followed, and historically reservoirs have

encountered significant regulatory and public challenges, regardless of the presence/absence of an existing impoundment.

### **Compensatory Mitigation**

The amount of mitigation potentially required for jurisdictional impacts within the Pumpkinvine Creek 02 project area was determined using the USACE's Standard Operating Procedure (SOP) for Compensatory Mitigation (March 2004). The SOP uses a series of factors such as location, type, existing condition, type of impact, etc. to generate a multiplying "factor." That factor is then multiplied by the impact area (acreage or linear footage) to calculate the required mitigation credits. Various conditions observed during the field surveys were used to calculate an average factor used to approximate required mitigation credits for impacts to jurisdictional features associated with the Pumpkinvine Creek 02 project area. *However, it is imperative to note that this document only serves as a guideline if impacts do not exceed 5,000 linear feet of stream or ten acres of wetland impacts.* Potential impacts for the Pumpkinvine Creek 02 exceed this threshold and actual compensatory mitigation requirements would likely be different from SOP estimates. Currently, the USACE Savannah District Office is developing a new SOP for large-scale projects focused on reservoirs. It is anticipated that this SOP would be issued mid-2008.

Utilizing the 2004 SOP and the approximated acreage and linear feet of jurisdictional waters located within the Pumpkinvine Creek 02 project area, an estimate of compensatory mitigation credits can be determined. Multiplying factors used for this analysis include: 6.7 for wetland systems, 5.7 for open waters, 12.7 for lower perennial streams, and 7.6 for intermittent streams. This factor was then multiplied by the acreage/ linear footage to determine an estimated number of mitigation credits required. The number of credits was multiplied by an average credit price to estimate the final estimated compensatory mitigation cost associated with the Pumpkinvine Creek 02. Refer to Table 6 located in the following section entitled "Project Construction Cost Estimate Narrative" for estimated impacts to jurisdictional waters and an estimate of mitigation credits required and associated costs.

### **Stream Buffer Variance**

The Georgia Erosion and Sedimentation Act of 1975 (GESA), as amended, requires that a 25-foot vegetated buffer be maintained along all state waters. Any land disturbing activities within the buffer would require obtaining a stream buffer variance from the EPD. The local issuing authority is responsible for determining if state waters are on-site and is responsible for determining if a stream buffer variance is required.

The GESA has a number of activities that are considered for stream buffer variances, including public water system reservoirs. Based on current regulations, reservoir construction would likely qualify for a variance. Attendant features such as pipelines and roadways, would likely be exempt from GESA regulations if stream crossings are constructed nearly perpendicular.

### **EPD Water Withdrawal Permit**

Georgia EPD requires a permit for withdrawal of 100,000 gallons per day or more of either surface water or ground water. In addition to justification of need for water for up to 50 years in the future, water withdrawal permits typically require the preparation of water conservation,

drought contingency, water supply/watershed protection, and reservoir management plans. A public hearing may be required as part of the withdrawal permitting process. EPD requires that its comments on the component plans be addressed before moving forward with issuing the water withdrawal permit. Based on previous permitting experience, a water withdrawal permit can be obtained within 5 to 7 months, depending on EPD's review time and the extent of their comments.

### **Source Water Protection Plan**

Amendments to the Federal Safe Drinking Water Act (SDWA) have brought about a new approach for ensuring clean and safe drinking water served by public water supplies in the United States. Management of a drinking water source now requires a Source Water Protection Plan. This plan basically defines watershed management strategies for ensuring that the water supply is not compromised by potential pollutant sources. Typically these sources are unmanaged development, but they can also include industrial sources that can potentially contaminate the water supply. The entity that operates this reservoir for water supply would be required to produce and implement the Plan. The Plan should also address any source water from outside the reservoir watershed that would be used to fill the reservoir, i.e., pumped/storage sources. The cost and schedule for producing a Source Water Assessment and the corresponding Source Water Protection Plan have not been included in any of the estimates presented in the report.

## PROJECT CONSTRUCTION COST ESTIMATE NARRATIVE

### Dam and Reservoir

The construction cost estimate for the proposed dam was based upon the general description provided in the background section of the report. Additionally, the following assumptions were made regarding the geometry of the dam.

- Upstream slope of 3H to 1V
- Downstream slope of 3H to 1V
- Upstream slope wave action protection in the form of riprap from 30 feet below the crest of the dam to 5 feet below the crest of the dam. Riprap supported by a berm located 30 feet below top of dam.
- Downstream slope having nearly horizontal 12-foot wide berms at 30-foot vertical intervals to control surface water runoff and erosion
- Crest of dam having a width of 25-feet

In addition to the above geometric considerations, the following internal drainage configurations were also considered in the estimation of construction costs.

- Chimney drain located at the downstream edge of the crest
- Trench drain located at 1/3 the distance from the downstream toe to the crest

A plan view and cross section of the proposed dam is provided in Figures 10 and 11.

Contained below are the items estimated to develop the construction cost estimate. We caution that the quantities and associated prices are based upon limited engineering evaluation and will likely change as the project proceeds into detailed evaluation and design.

#### Mobilization and Demobilization

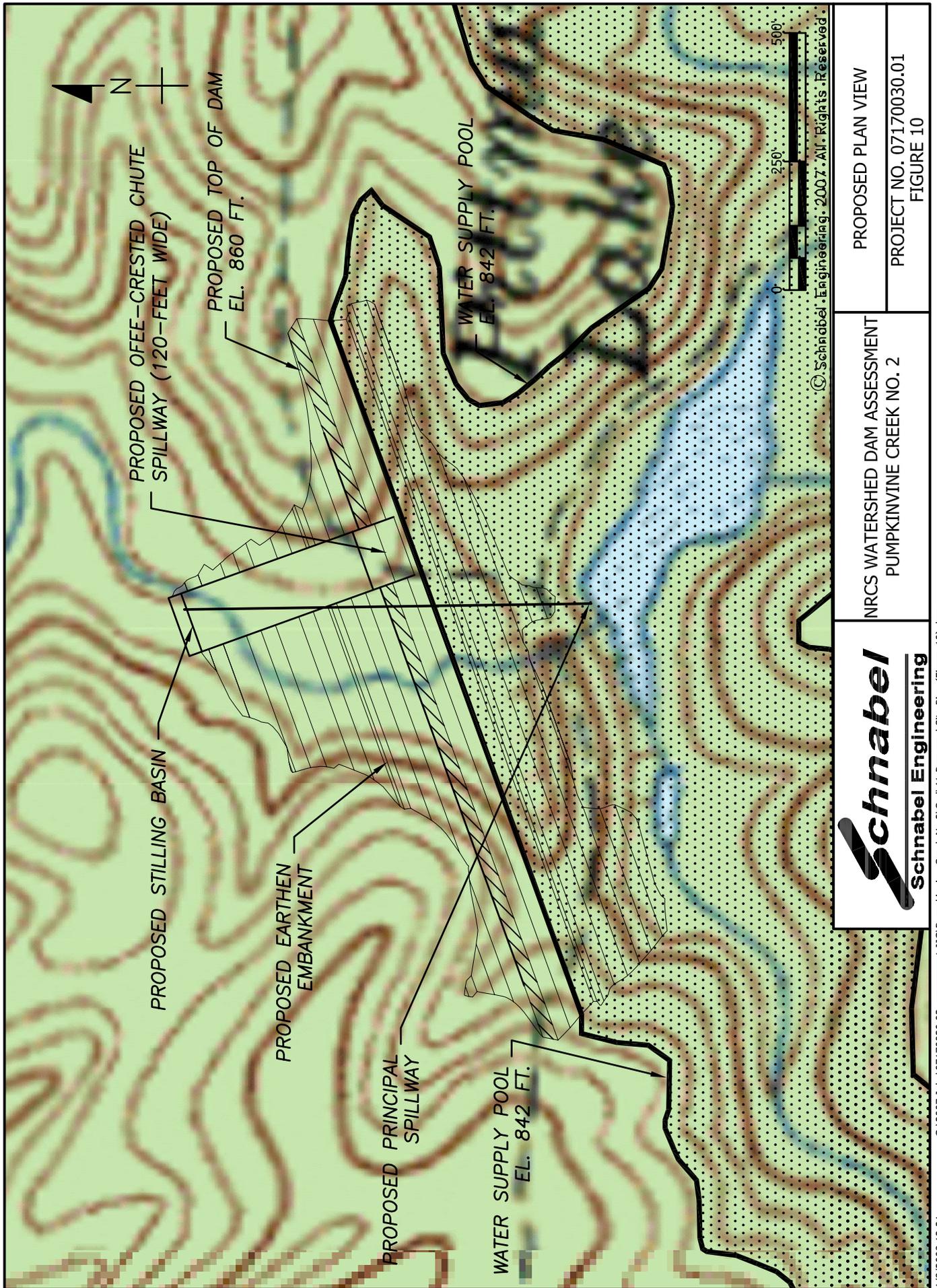
Mobilization and demobilization is a lump sum item estimated at 6 percent of the unit rate sum of the construction items.

#### Erosion and Sedimentation Control

Erosion and sedimentation control is a lump sum item estimated at 2 percent of the sum of unit rate construction items.

#### Control of Water

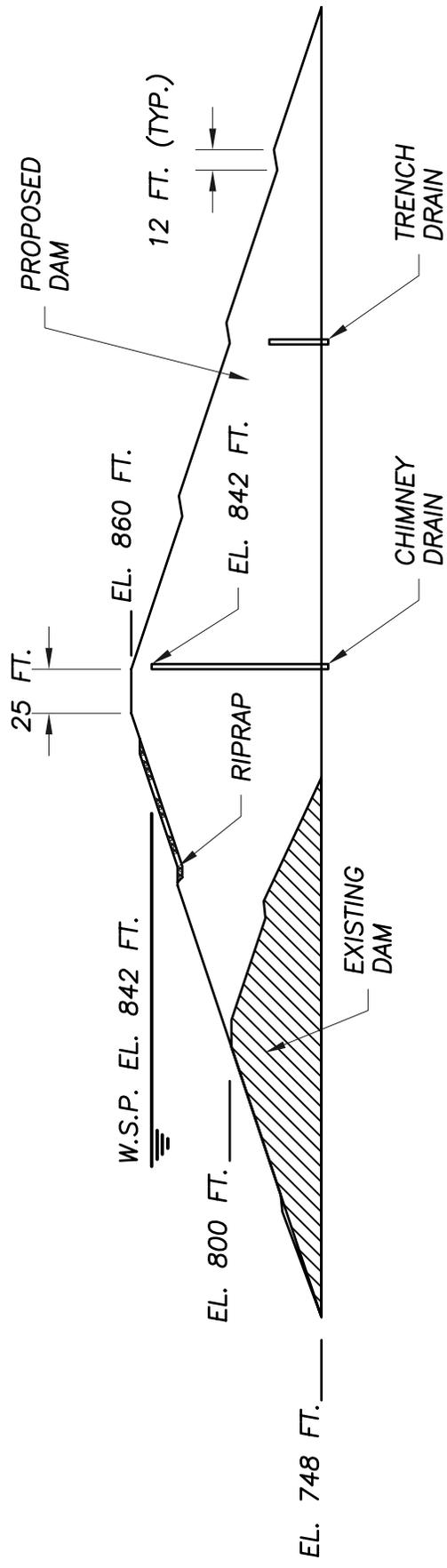
Control of water is a lump sum item estimated at 3 percent of the sum of unit rate construction items. This item includes the control of both surface water and groundwater and will likely consist of stream diversion, cofferdam construction and maintenance, pumping, and well points, as well as any other means of controlling water during construction.



NRCS WATERSHED DAM ASSESSMENT  
PUMPKINVINE CREEK NO. 2

PROPOSED PLAN VIEW

PROJECT NO. 07170030.01  
FIGURE 10



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	<p>NRCS WATERSHED DAM ASSESSMENT PUMPKINVINE CREEK NO. 2</p>	<p>TYPICAL SECTION</p>
<p>PROJECT NO. 07170030.01 FIGURE 11</p>		

## Clearing

Clearing is a unit rate item measured in acres associated with the removal of trees and other vegetation from the reservoir. The estimated area of clearing was assumed to be equal to the surface area of the reservoir at the normal pool elevation.

## Clearing and Grubbing

Clearing and grubbing is a unit rate item measured in acres associated with the removal of trees, other vegetation, and associated root mats in the areas to receive structural fill or concrete. The estimated area of clearing and grubbing was assumed to be equal to the footprint of the proposed dam plus an additional 50-foot perimeter around the proposed dam.

## Earth Fill

Earth Fill is a unit rate item measured in cubic yards. The computed volume of earth fill represents the estimated quantity required to construct the dam as described herein. The estimated quantity was computed using an AutoCad Civil 3D computer model based on the proposed grading and existing topography. In addition to the proposed embankment earth fill, foundation excavation backfill was calculated (see Excavation, Common for details) and added to the embankment earth fill to determine the total quantity of earth fill.

## Drain Fill

Drain Fill is a unit rate item measured in cubic yards. The computed volume of drain fill represents the estimated quantity of fine and coarse-grained drain material required to construct the internal drainage system as described herein. For the purposes of this study, no differentiation was made between fine and coarse drain fill. In addition, the quantity for the trench drain was assumed to be equal to half of the chimney drain quantity. The chimney drain was assumed to have a top elevation equal to the proposed normal pool elevation and a bottom elevation approximated at the limits of the foundation excavation. The chimney drain was assumed to have a width of three feet and run the length of the dam from one abutment, into the floodplain, and up the other abutment tying into residual soils.

## Excavation, Common

Excavation, Common is a unit rate item measured in cubic yards associated with the removal of unsuitable material (soils) within and adjacent to the footprint of the proposed dam. The volume of common excavation was calculated by approximating the surface area of the floodplain within the limits of clearing and grubbing as well as the depth of excavation within the same area. The surface area of the floodplain was approximated using available topographic maps. The depth of excavation was estimated from the boring data included in the design plans for the existing dam.

## Riprap

Riprap is a unit rate item measured in tons. The computed weight of riprap represents the estimated quantity required to construct the wave-action berm as described herein. Riprap was

assumed to be placed on the upstream slope of the dam. The section of riprap was assumed to extend 30 vertical feet, have a thickness of about 2-¾ feet, and traverse the length of the proposed dam.

#### Permanent Turf Establishment

Permanent Turf Establishment is a unit rate item measured in acres associated with the establishment of a permanent turf at the conclusion of construction activities for the proposed dam. The estimated area of permanent turf establishment was assumed to be equal to the estimated area of clearing and grubbing.

#### Concrete, Class 4000

Concrete, Class 4000 is a unit rate item measured in cubic yards associated with the construction of the reinforced concrete auxiliary chute spillway. The volume of concrete was estimated by comparing the proposed auxiliary spillway drop in elevation and width to the drops in elevation and widths of constructed reinforced concrete chute spillways. A relationship was developed between the drop in elevation and width of the constructed spillways and the required quantity of concrete. This relationship was applied to the proposed dam to estimate the quantity of concrete.

#### Principal Spillway Reinforced Concrete Pressure Pipe

Reinforced Concrete Pressure Pipe (RCPP) is a unit rate item measured in feet. The computed length of RCPP represents the estimated quantity required to construct the principal spillway conduit described herein. The RCPP was assumed to be placed through the base of the proposed dam from the upstream toe to the downstream toe. The diameter of the pipe was assumed to be equal to the diameter of the pipe in the existing dam.

#### Concrete, Class 3000 (mass)

Concrete, Class 3000 is a unit rate item measured in cubic yards associated with the construction of the concrete cradle beneath the principal spillway pipe. The concrete cradle was assumed to be designed as a Soil Conservation Service Type A2 cradle and run the length of the principal spillway pipe minus ten feet.

#### Reinforced Concrete Riser

The Reinforced Concrete Riser is a lump sum item associated with the construction of the reinforced concrete principal spillway structure. The cost was estimated by comparing the proposed principal spillway riser height to the heights of constructed reinforced concrete riser structures. A relationship was developed between the height of the constructed spillways and the cost to construct them. This relationship was utilized to estimate the cost of the proposed riser structure.

#### **Land Acquisition**

The costs associated with land acquisitions are unit rate items based upon the number of acres that will need to be purchased at the top-of-dam elevation, the number of acres that will need to

be managed for a 150-foot buffer around the normal pool, and the number of houses that will need to be purchased. For the purposes of the buffer management, only the portions of the buffer above top-of-dam elevation were considered. The costs to purchase the land were estimated based upon available records of recent land sales. The cost to manage the buffer was assumed to be 60 percent of the land purchase cost. The cost of each structure impacted was assumed to be \$200,000.

### **Roadway Relocation**

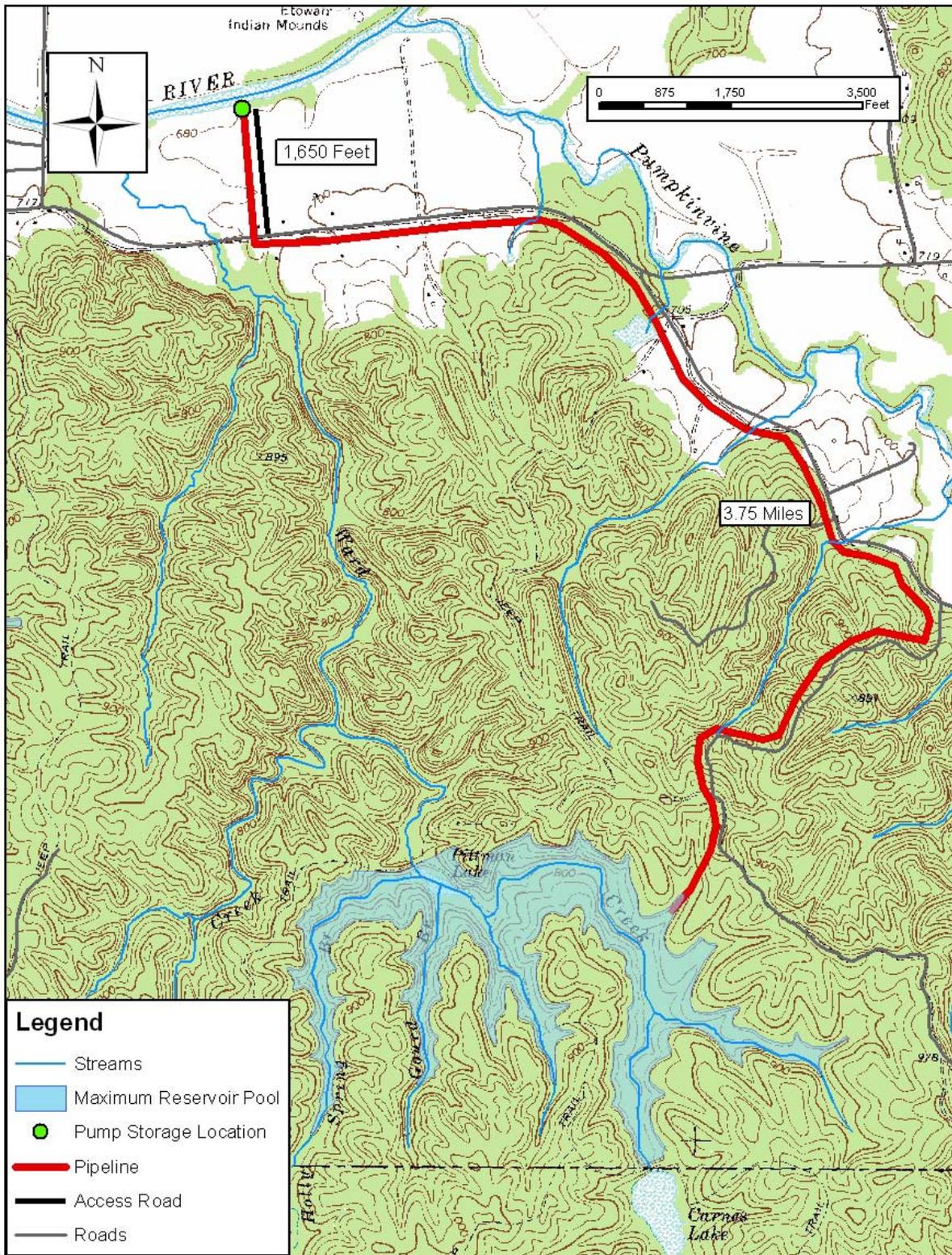
To construct the proposed project, no roads will be impacted.

### **Pump Station and Pipeline Cost Estimation**

The pump storage location for Pumpkinvine Creek Reservoir 02 is located on the Etowah River, downstream of its confluence with Pumpkinvine Creek as shown in Figure 12. The reservoir is located along Ward Creek, approximately 2.5 miles upstream of the confluence with the Etowah River. With a water supply pool elevation of 842 feet, Pumpkinvine Creek Dam 02 has an average day yield of approximately 6.8 MGD. A 30-inch ductile iron pipe (DIP) was selected to carry water from the pump storage location to the reservoir. This pipeline is approximately 3.75 miles in length and will pump water from the storage location elevation of 675 feet, to the 842 feet height of the reservoir water surface. A cascading structure will need to be constructed where the pipe comes into the reservoir to provide aeration and erosion control.

Four 4-MGD pumps were selected at the pump storage location to pump water to the reservoir. This gives a firm pumping capacity of 12-MGD, which is roughly twice the daily yield of the reservoir, the standard assumption for pump capacity. This pumping capacity will allow the reservoir to remain stable during times of peak water demand, as well as give redundancy in the case of failure in one of the pumps. An access road will need to be constructed in order to construct and maintain the pumping station on the Etowah River. This road will run approximately 0.3 miles from Old Alabama Road. The cost opinion for these components is found in the appendix.

**Figure 12**  
**Project Location Map**



## Compensatory Mitigation

The simplest mitigation option is typically purchasing credits from a bank. Compensatory mitigation credits may be purchased from an approved mitigation bank or through the Georgia Land Trust Service Center if a bank is not available within the project area. Based on recent projects, wetland credits range from \$7,000-\$10,000 per credit and stream credits range from \$70-\$110 per credit. An alternative to purchasing credits is obtaining credits by conducting on-site restoration or preservation of jurisdictional waters.

**Table 6**  
**Pumpkinvine Creek 02 Estimated Impacts and Overall Mitigation Banking Cost Analysis**

<b>Impact Type</b>	<b>Estimated Impact Acres(ac)/Linear Feet (ft)</b>	<b>Projected Credits Needed</b>	<b>Projected Cost* \$90/stream credit \$7,500/wetland credit</b>
Wetland	11.87 ac	90	\$675,000
Intermittent Stream	744 ft	5,654	\$508,860
Lower Perennial Stream	19,896 ft	252,679	\$22,741,110
Open Water	5.7 ac	16	\$120,000
<b>Total</b>	<b>14.65 acres / 20,640 ft</b>	<b>346 wetland / 258,333 stream**</b>	<b>\$24,044,970</b>

\*Cost is based on recent quotes from banks within the Etowah River Basin. Actual banking price may be higher or lower than estimated depending on the date of purchase and credit availability.

\*\*Total required credits calculated using the March 2004 Standard Operating Procedure mitigating guidelines established by the US Army Corps of Engineers, which only serves as a guideline for large projects.

## Estimated Project Construction Cost

The total project cost is estimated at \$78,000,000. Table A-5, located in the appendix, shows an itemized breakdown of the costs associated with enlarging the existing dam and reservoir. These costs are estimates and are based on multiple assumptions.

## **APPENDIX**

### **FIGURES**

Figure A-1a	Calculation of Stage Storage / Stage Area Curves
Figure A-1b	Stage Storage / Stage Area Curves
Figure A-2	Regression Equations for Area to Storage and Depth to Storage
Figure A-3	Storage vs. Time and Elevation vs. Time for Assumed Safe Yield

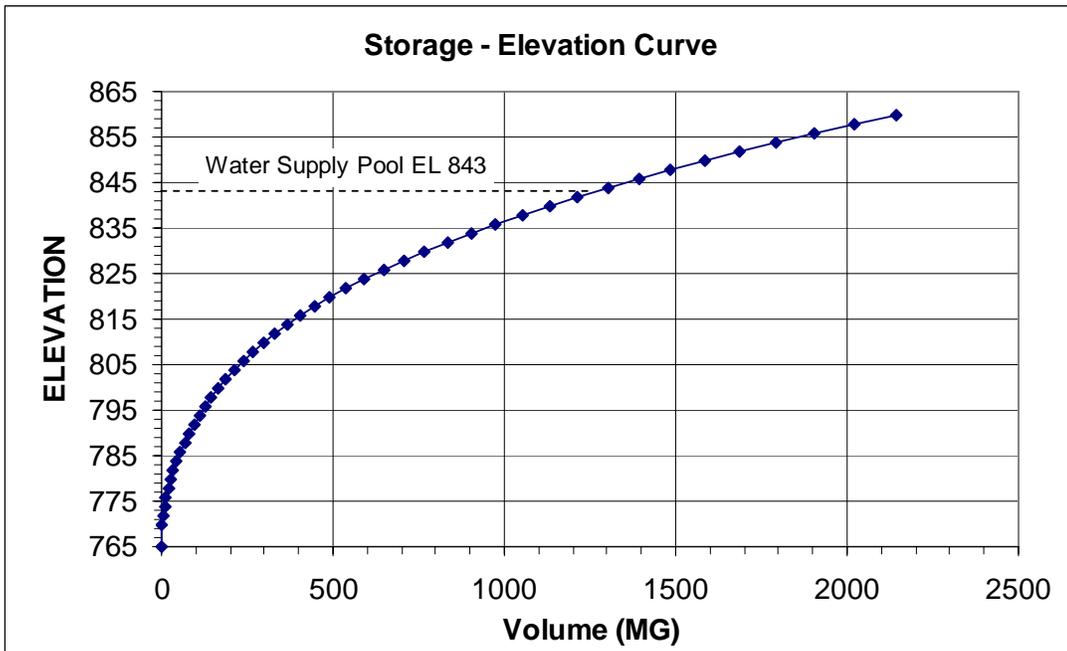
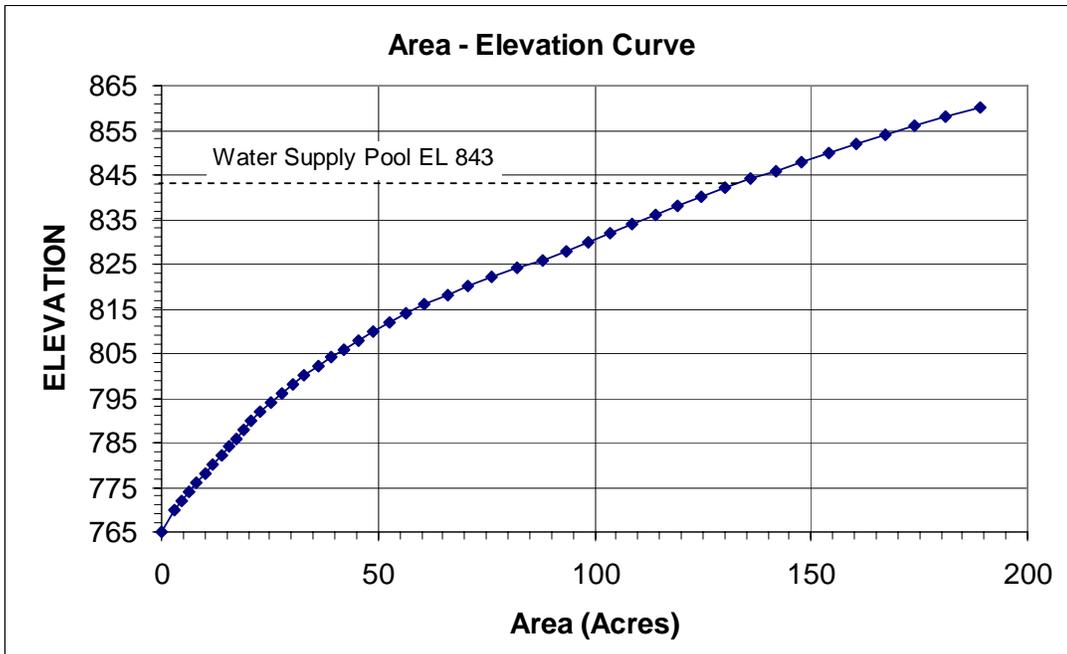
### **TABLES**

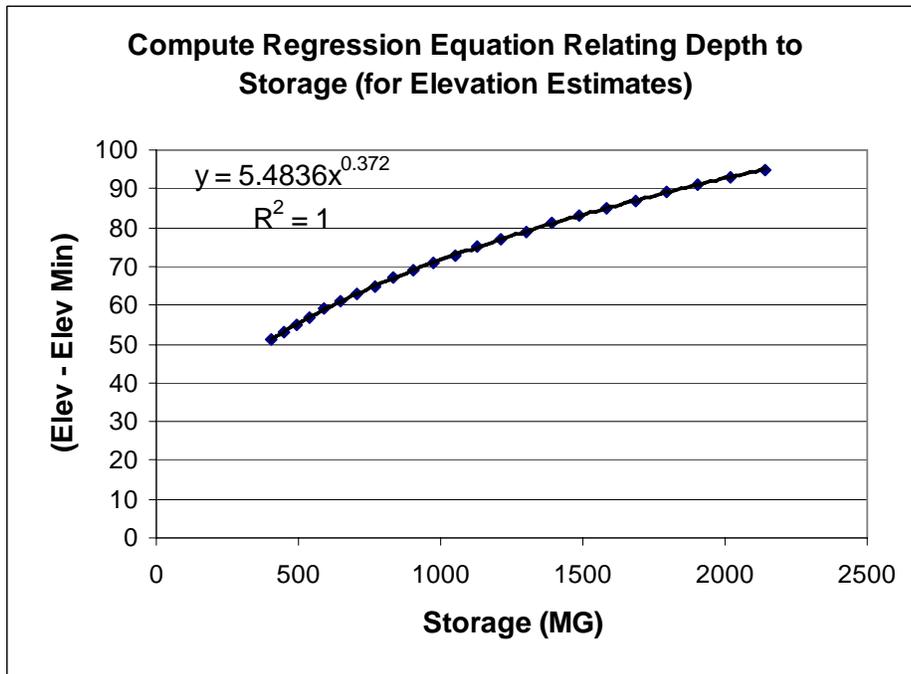
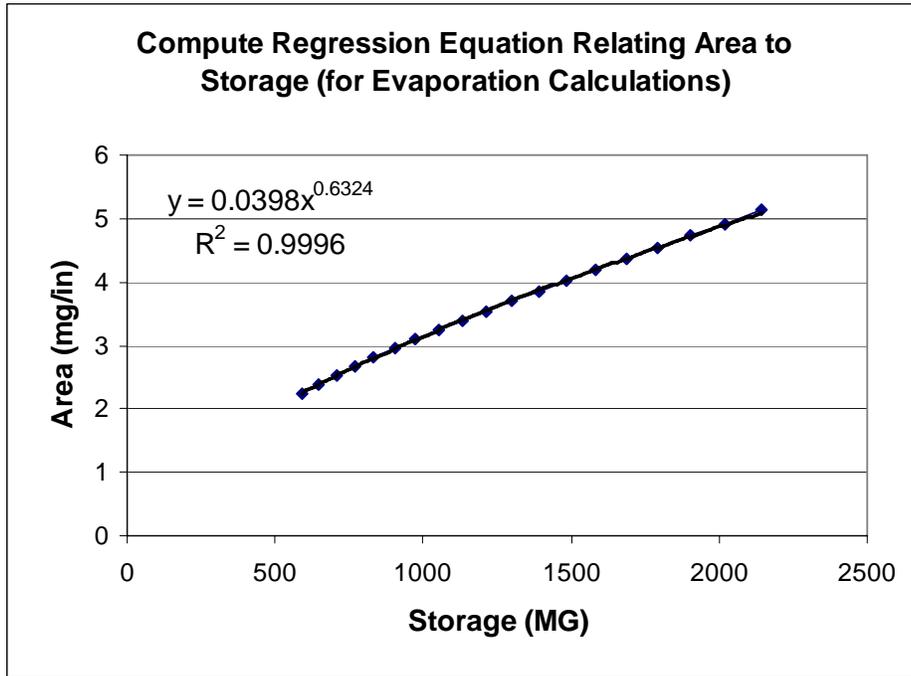
Table A-1	Summary of Opinion of Probable Construction Costs for Pumping Facilities and Pipelines
Table A-2	Opinion of Probable Construction Costs – River Intake and Pump Station
Table A-3	Opinion of Probable Construction Costs – 30-inch Raw Water Line
Table A-4	Opinion of Probable Construction Costs – Reservoir Inlet Structure
Table A-5	Total Project Opinion of Cost

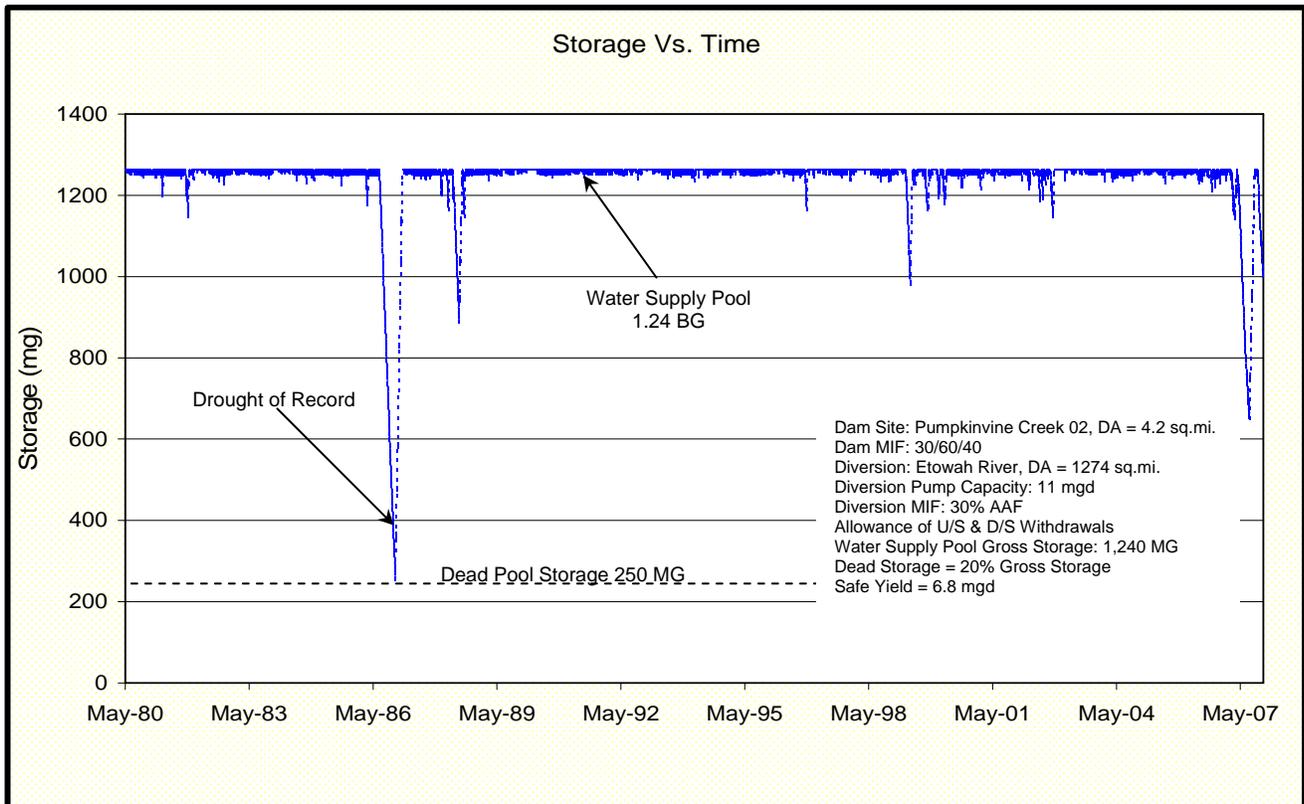
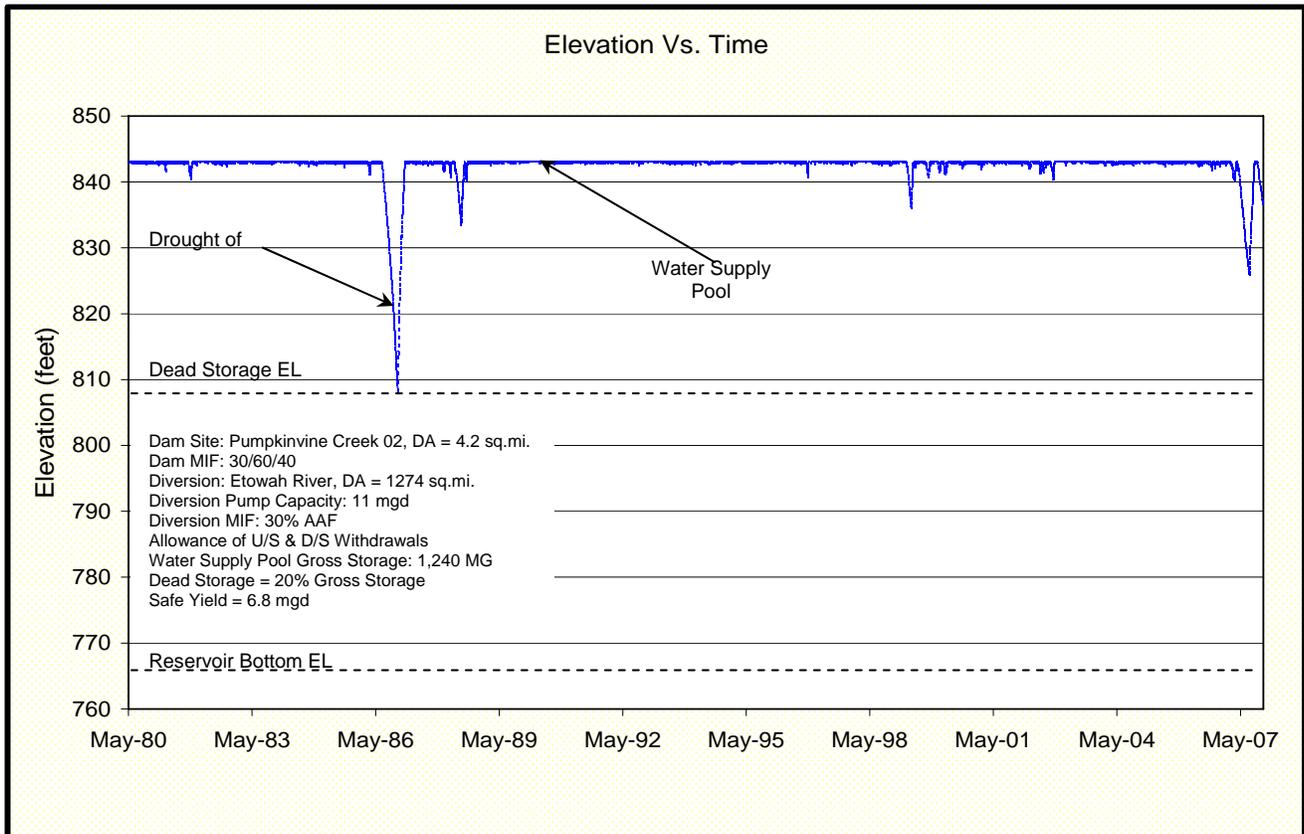
Figure A-1a

Pumpkinvine Creek 02  
Area and Storage Curves

Elev.	Area Acres	Area mg/in	Inc. Vol.		Cumulative Vol	
			A-FT	A-FT	A-FT	M Gal.
765	0	0	0	0	0	0
770	2.84	0	7	7	7	2
772	4.62	0	7	15	15	5
774	6.48	0	11	26	26	8
776	8.17	0	15	40	40	13
778	10.07	0	18	59	59	19
780	11.76	0	22	80	80	26
782	13.75	0	26	106	106	35
784	15.52	0	29	135	135	44
786	17.34	0	33	168	168	55
788	19.03	1	36	204	204	67
790	20.83	1	40	244	244	80
792	22.87	1	44	288	288	94
794	25.23	1	48	336	336	110
796	27.76	1	53	389	389	127
798	30.21	1	58	447	447	146
800	32.95	1	63	510	510	166
802	36.14	1	69	579	579	189
804	39.11	1	75	655	655	213
806	42.11	1	81	736	736	240
808	45.33	1	87	823	823	268
810	48.88	1	94	917	917	299
812	52.49	1	101	1019	1019	332
814	56.46	2	109	1128	1128	368
816	60.65	2	117	1245	1245	406
818	65.97	2	127	1371	1371	447
820	70.64	2	137	1508	1508	491
822	76.11	2	147	1655	1655	539
824	82.07	2	158	1813	1813	591
826	88.07	2	170	1983	1983	646
828	93.37	3	181	2165	2165	705
830	98.52	3	192	2356	2356	768
832	103.67	3	202	2559	2559	834
834	108.76	3	212	2771	2771	903
836	113.90	3	223	2994	2994	976
838	119.14	3	233	3227	3227	1052
840	124.58	3	244	3471	3471	1131
842	130.25	4	255	3725	3725	1214
844	136.08	4	266	3992	3992	1301
846	141.93	4	278	4270	4270	1391
848	147.84	4	290	4559	4559	1486
850	154.00	4	302	4861	4861	1584
852	160.55	4	315	5176	5176	1687
854	167.21	5	328	5504	5504	1794
856	174.03	5	341	5845	5845	1905
858	181.26	5	355	6200	6200	2021
860	189.02	5	370	6570	6570	2141







**WATERSHED DAM ASSESSMENT - PUMPKINVINE CREEK 02**

Bartow County, Georgia (7194-001)

**OPINION OF PROBABLE CONSTRUCTION COST ESTIMATE - CONCEPTUAL LEVEL**

Summary by Division

TABLE A-1

Division	01 - Water Intake and Pump Station and Access Road	02 - 30 - inch Raw Water Force Main and Venturi Vault	03 - Reservoir Inlet Structure	TOTAL	% of Total	
1	\$0.57	\$0.29	\$0.05	\$0.92	8.64%	<b>PUMPKINVINE CREEK 02:</b> Maximum Safe Reservoir Yield: 6.8 MGD RWPS Firm Pumping Capacity: 11.0 MGD RWFPM Pipe Diameter: 30-inches
2	\$0.80	\$0.00	\$0.04	\$0.84	7.92%	
3	\$0.76	\$0.02	\$0.27	\$1.05	9.85%	
4	\$0.07	\$0.00	\$0.00	\$0.07	0.67%	
5	\$0.02	\$0.00	\$0.00	\$0.02	0.21%	
6	\$0.00	\$0.00	\$0.00	\$0.00	0.00%	
7	\$0.02	\$0.00	\$0.00	\$0.02	0.15%	
8	\$0.03	\$0.00	\$0.00	\$0.03	0.28%	
9	\$0.05	\$0.00	\$0.00	\$0.05	0.47%	
10	\$0.00	\$0.00	\$0.00	\$0.00	0.00%	
11	\$1.13	\$0.00	\$0.06	\$1.19	11.17%	
12	\$0.00	\$0.00	\$0.00	\$0.00	0.00%	
13	\$0.00	\$0.00	\$0.00	\$0.00	0.00%	
14	\$0.09	\$0.00	\$0.00	\$0.09	0.86%	
15	\$0.41	\$2.91	\$0.01	\$3.33	31.38%	
16	\$0.76	\$0.06	\$0.00	\$0.81	7.63%	
17	\$0.15	\$0.02	\$0.00	\$0.17	1.60%	
Structure Contingency	\$0.49	\$0.00	\$0.00	\$0.49	4.58%	
Markup	\$0.90	\$0.56	\$0.09	\$1.55	14.58%	
<b>Structure Total (without Contingency)</b>	<b>\$6.24</b>	<b>\$3.85</b>	<b>\$0.53</b>	<b>\$10.61</b>	<b>100.00%</b>	
<b>Project Contingency</b>	<b>\$1.87</b>	<b>\$1.15</b>	<b>\$0.16</b>	<b>\$3.18</b>	<b>30.00%</b>	
<b>Structure Total (with Contingency)</b>	<b>\$8.11</b>	<b>\$5.00</b>	<b>\$0.68</b>			
<b>All Figures are in Millions</b>	<b>PROJECT TOTAL</b>			<b>\$13.80 M</b>		



**WATERSHED DAM ASSESSMENT - (7194-001)  
PUMPKINVINE CREEK 02**

02  
DECEMBER 2007

**OPINION OF PROBABLE CONSTRUCTION COST ESTIMATE - CONCEPTUAL LEVEL**

TABLE A-3

02 - 30-inch Raw Water Line

No.	Spec. Sect.	Description	Unit	Qty	Labor \$\$		Material \$\$		Equipment \$\$		Subcontractor \$\$		Total
					Unit	Total	Unit	Total	Unit	Total	Unit	Total	
<b>02 - 30-inch Raw Water Line with Venturi Vault</b>													
<b>Div 1</b>													
1	1000	General Conditions	LS	1		\$107,000		\$77,400		\$107,200		\$0	\$291,600
<b>Div 2</b>													
2	2125	Erosion and Sedimentation Control Maintenance - with Unit Bid	MTH			\$0		\$0		\$0		\$0	\$0
3		Dewatering	LS			\$0		\$0		\$0		\$0	\$0
4	2510	Asphalt Concrete Pavement - with Unit Bid	LS			\$0		\$0		\$0		\$0	\$0
5	2523	Concrete Sidewalk and Curbs - with Unit Bid	LS			\$0		\$0		\$0		\$0	\$0
<b>Div 3</b>													
6	3300	Miscellaneous Concrete (Venturi Vault)	LS	1	\$1,500.00	\$1,500	\$12,500.00	\$12,500	\$1,000.00	\$1,000	\$0.00	\$0	\$15,000
<b>Div 4</b>													
<b>Div 5</b>													
<b>Div 6</b>													
<b>Div 7</b>													
<b>Div 8</b>													
<b>Div 9</b>													
<b>Div 10</b>													
<b>Div 11</b>													
<b>Div 12</b>													
<b>Div 13</b>													
<b>Div 14</b>													
<b>Div 15</b>													
7		<b>30" DIP</b>	<b>Depth</b>	<b>7</b>	<b>Depth of Cover</b>		<b>4</b>						
8		30" Pipe Excavation - Earth (compacted volume)	CY	19663	\$0.75	\$14,747		\$0	\$3.00	\$58,988		\$0	\$73,734
9		30" Pipe Excavation - Trench Rock (compacted volume)	CY	6554		\$0		\$0		\$0	\$35.00	\$229,396	\$229,396
10		Trench Box	LF	19,800		\$0	\$1.00	\$19,800		\$0		\$0	\$19,800
11		30" DIP Pressure Class 200	LF	15,900	\$7.67	\$121,889	\$80.26	\$1,276,070	\$2.50	\$39,750		\$0	\$1,437,710
12		30" Pipe Bedding (compacted volume)	CY	4,033	\$1.00	\$4,033	\$13.00	\$52,433	\$1.00	\$4,033		\$0	\$60,500
13		30" Pipe Backfill (compacted volume)	CY	18,584	\$1.00	\$18,584		\$0	\$4.00	\$74,334		\$0	\$92,918
14		Import Backfill Materials (loose volume, assume 10% swell)	CY	1,187		\$0	\$13.00	\$15,428		\$0		\$0	\$15,428
15		Haul off Rock (assume 15% swell) - with Unit Bid	CY	7,537		\$0		\$0		\$0	\$15.00	\$113,059	\$113,059
16		30" 90-degree Bend	EA	2	\$190.00	\$380	\$5,340.60	\$10,681	\$50.00	\$100		\$0	\$11,161
17		30" 45-degree Bend	EA	6	\$190.00	\$1,140	\$4,181.40	\$25,088	\$50.00	\$300		\$0	\$26,528
18		30" 22.5-degree Bend	EA	12	\$190.00	\$2,280	\$3,709.44	\$44,513	\$50.00	\$600		\$0	\$47,393
19		30" 11.25-degree Bend	EA	6	\$190.00	\$1,140	\$3,436.20	\$20,617	\$50.00	\$300		\$0	\$22,057
20		30" DIP Pressure Class 200 RJ	LF	3,900	\$9.17	\$35,747	\$109.82	\$428,314	\$2.50	\$9,750		\$0	\$473,811
21													
22		Earthwork Calculations				\$0		\$0		\$0		\$0	\$0
23		Pipe Excavation - Total Compacted Volume	CY	26217		\$0		\$0		\$0		\$0	\$0
24		Rock - Total Compacted Volume (assume 25% of excavation)	CY	6554		\$0		\$0		\$0	\$37.00	\$242,504	\$242,504
25		Pipe Bedding - Total Compacted Volume	CY	4033		\$0		\$0		\$0		\$0	\$0
26		Pipe Backfill - Total Compacted Volume Needed	CY	18584		\$0		\$0		\$0		\$0	\$0
27		On-Site Backfill Material Available - Compacted Volume	CY	19663		\$0		\$0		\$0		\$0	\$0
28		Materials for Disposal - Compacted Volume	CY	1079	\$5.00	\$5,395		\$0	\$5.00	\$5,395		\$0	\$10,789
29													
30		Air Release Valve and Manhole (3 each)	LS	1	\$2,200.00	\$2,200	\$26,400.00	\$26,400	\$1,800.00	\$1,800	\$0.00	\$0	\$30,400
31													
<b>Div 16</b>													
32	16000	Electrical	LS	1		\$0		\$0		\$0	\$55,000.00	\$55,000	\$55,000
<b>Div 17</b>													
33	17000	Venturi Meter	LS	1	\$1,000.00	\$1,000	\$10,500.00	\$10,500	\$500.00	\$500		\$0	\$12,000
34	17000	Instrumentation	LS	1		\$0		\$0		\$0	\$7,500.00	\$7,500	\$7,500
		Contingency	LS	0%		\$0		\$0		\$0		\$0	\$0
		Subtotals				\$317,035		\$2,019,746		\$304,050		\$647,459	\$3,288,290
Sales Tax @					7.0%	\$141,400	<b>Assumptions:</b>						
Labor Burden @					30.0%	\$95,100	Estimate DOES NOT include easements acquisitions, land acquisitions or mitigations required to build the pump station						
Bonds On Subs @					1.5%	\$9,700	Assumed 25% of the excavated material is rock						
Subtotal						\$3,534,490							
Fee @					7.0%	\$247,400							
Insurance & Bonds @					1.7%	\$64,300							
<b>Estimated Construction Cost</b>						<b>\$3,846,190</b>	<b>\$194 per LF</b>						



Table A-5

**Pumpkinvine Creek Dam No. 10****TOTAL PROJECT OPINION OF COST**

<b><u>Item No.</u></b>	<b><u>Description of Work</u></b>	<b><u>Estimated Quantity</u></b>	<b><u>Lump Sum</u></b>	<b><u>Lump Sum Price</u></b>	<b><u>Amount</u></b>
1.	Mobilization and Demobilization	1	Job	<u>Lump Sum</u>	<u>\$762,817</u>
2.	Erosion & Sediment Control	1	Job	<u>Lump Sum</u>	<u>\$254,272</u>
3.	Control of Water	1	Job	<u>Lump Sum</u>	<u>\$381,408</u>
4.	Clearing	130	Ac	<u>\$2,500</u>	<u>\$325,000</u>
5.	Clearing & Grubbing	18	Ac	<u>\$5,000</u>	<u>\$90,000</u>
6.	Earth Fill	830,041	Cu-Yd	<u>\$4</u>	<u>\$3,320,164</u>
7.	Drain Fill	12,634	Cu-Yd	<u>\$75</u>	<u>\$947,550</u>
8.	Excavation, Common	37,324	Cu-Yd	<u>\$5</u>	<u>\$186,620</u>
9.	Riprap	19,781	Ton	<u>\$75</u>	<u>\$1,483,575</u>
10.	Permanent Turf Establishment	18	Ac	<u>\$2,000</u>	<u>\$36,000</u>
11.	Concrete, Class 4000 (reinforced)	6,808	Cu-Yd	<u>\$850</u>	<u>\$5,786,800</u>
12.	Concrete, Class 3000 (mass)	158	Cu-Yd	<u>\$400</u>	<u>\$63,200</u>
13.	24-Inch RCP	842	Feet	<u>\$350</u>	<u>\$294,700</u>
14.	Principal Spillway Riser	1	Lump Sum	<u>\$180,000</u>	<u>\$180,000</u>
<b><u>Dam Construction Cost Estimate</u></b>					<b><u>\$14,112,106</u></b>
15.	30-Inch Pipeline	1	Lump Sum	<u>\$3,850,000</u>	<u>\$3,850,000</u>
16.	Cascading Structure	1	Lump Sum	<u>\$530,000</u>	<u>\$530,000</u>

17.	Pumping Station (Including Raw Water Pumps and Access Road)	1	Lump Sum	<u>\$6,240,000</u>	<u>\$6,240,000</u>
	<b>Pump Station and Pipeline Cost Estimate</b>				<b><u>\$10,620,000</u></b>
18.	Land Acquisition	189	Ac	<u>\$30,000</u>	<u>\$5,670,000</u>
19.	Easement Acquisition	77	Ac	<u>\$18,000</u>	<u>\$1,382,220</u>
20.	Building Acquisition	0	Buildings	<u>\$200,000</u>	<u>\$0</u>
	<b>Land Acquisition Cost Estimate</b>				<b><u>\$7,052,220</u></b>
21.	Wetland	90	Credits	<u>\$7,500</u>	<u>\$675,000</u>
22.	Intermittent Stream	5,654	Credits	<u>\$90</u>	<u>\$508,860</u>
23.	Lower Perennial Stream	252,679	Credits	<u>\$90</u>	<u>\$22,741,110</u>
24.	Open Water	16	Credits	<u>\$7,500</u>	<u>\$120,000</u>
	<b>Impacts and Overall Mitigation Cost Estimate</b>				<b><u>\$24,044,970</u></b>
	<b><u>Construction, Land Acquisition, Mitigation Estimate</u></b>				<b><u>\$55,829,296</u></b>
	<b><u>Contingency at 25%</u></b>				<b><u>\$13,957,324</u></b>
	<b><u>Professional Services at 15% *</u></b>				<b><u>\$8,374,394</u></b>
	<b><u>Total Project Estimate</u></b>				<b><u>\$78,161,014</u></b>
	<b><u>Suggested Project Estimate</u></b>				<b><u>\$78,000,000</u></b>

\*Professional services include but are not limited to engineering, construction management legal, appraisals, and environmental consulting.